#### National Examinations – May 2017

#### 16-Civ-A6, Highway Design, Construction and Maintenance

#### 3 Hour Duration

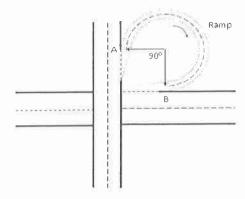
#### **NOTES**

- 1. If doubt exists as to the interpretation of any question, the candidate is urged to submit with the answer paper a clear statement of any assumptions made.
- 2. Any data, not given but required, can be assumed.
- 3. This is a "CLOSED BOOK" examination. Candidates may use one of two calculators, the Casio or Sharp approved models.
- 4. A total of **five** solutions is required. Only the first five as they appear in your answer book will be marked.
- 5. All questions are of equal value.
- 6. For non-numerical questions, clarity and organization of the answer are important.

### **Marking Scheme**

- 1. (a) 8 marks; (b) 8 marks; (c) 4 marks
- 2. (a) 8 marks; (b) 8 marks; (c) 4 marks
- 3. (a) 15 marks; (b) 5 marks
- 4. (a) 15 marks; (b) 5 marks
- 5. (a) 8 marks; (b) 8 marks; (c) 4 marks
- 6. (a) 15 marks; (b) 5 marks
- 7. (a) 10 marks; (b) 10 marks

- 1. You are asked to design a ramp of an interchange connecting two freeways as shown in the following figure. The ramp has two lanes and each lane has a lane width of 3.6 m. The elevation difference between point A (overpass) and point B is 5 m. A simple curve is to be used with a design speed of 30 km/h and a superelevation of 0.08 on this ramp.
  - a) What is the minimum radius required for this ramp (measured from the center line of the two lanes)?
  - b) If the minimum radius calculated in (a) is used, what distance must be cleared from the inside edge of the ramp to provide adequate stopping sight distance?
  - c) If the minimum radius calculated in (a) is used and the stationing of the Point of Tangent (PT) is 90 + 00, determine the stationing of the Point of Curve (PC).



- 2. You are asked to design a horizontal curve for a two-lane two-way highway with a design speed of 80 km/h. The curve is located on 2% grade (Note that the inside lane is up grade) at a Point of Intersection with a central angle of 30°. The highway has 3.6-m lanes. Local guidelines dictate a maximum superelevation of 8%. A preliminary design has suggested a radius of 240 m for this curve.
  - a) Verify that the recommended radius is safe for vehicles to negotiate the curve at the design speed.
  - b) Due to expensive excavation, it is determined that a maximum of 6 meters can be cleared from the roads centerline, what speed limit should be imposed at this location?
  - c) If the stationing of the Point of Intersection (PI) is 100 + 00, determine the stationing of the Point of Tangent (PT).
- 3. A vehicle was traveling at 80 km/h on a parabolic crest vertical curve section on a rural highway. A stalled vehicle was spotted on the same curve section and the drive immediately took action to stop the vehicle. Unfortunately he struck the stalled vehicle at a speed of 5 km/h. An after-accident investigation reveals that the curve connects a +3% grade to the -3% grade, and has a length of 270 m. The design speed of this highway is 80km/h. The vehicle has an eye height of 1.08 m and the stalled vehicle has a height of 1.10 m. A series of test runs show that the coefficient of friction is 0.32.
  - a) The driver later claimed that there was not enough sight distance available at this section. Would you agree with him?
  - b) What could be the other factors that had contributed to the accident?

- 4. You are asked to design a flexible pavement structure for a new two-lane, two-way highway. The following information and design requirements are made available to you:
  - The pavement should last for 15 years with a minimum PSI of 2.5 at a probability of 70% or higher. The initial PSI is 4.5 and overall standard deviation is 0.40.
  - Several in-situ modulus tests show that the subgrade has an effective soil resilient modulus of 4000psi.
  - The traffic on this highway is composed entirely of trucks with a daily volume of 120 trucks per lane for the first year. The predicted traffic growth rate is 5.0%. Each truck has one 18-kip single axle and one 30 kip tandem axle.
  - The paving materials that are economically available for this highway includes hot-mix asphalt concrete, soil-cement and crushed stone.
  - ASSHTO pavement design method was designated as the official design method.

The proposed pavement structure consists of a 4-in. hot-mix asphalt concrete wearing surface, a 6-in. Soil-cement base, and a 10-in. crushed stone subbase.

- a) Determine whether or not the design is appropriate neither over-designed nor underdesigned. Make sure to justify your conclusion.
- b) Explain how various environmental factors are considered in AASHTO pavement design method?
- 5. Briefly Answer the Following Questions:
  - a) Engineer A was asked to design a RIGID pavement structure as an alternative to a FLEXIBLE pavement structure prepared by his fellow Engineer B. AASHTO design method were used for designing both rigid and flexible pavements. Engineer A decided to use some data from Engineer B's design, including the cumulative ESAL's. Is it acceptable for Engineer A to do so? Why or why not?
  - b) During a pavement design process using AASHTO method, an engineer noticed that the LEF value of a 40-kip tandem axle load for SN=5 is higher than for SN=4. He/she then concluded that the axle load may cause a higher damage to a pavement with a higher SN than to a pavement with a lower SN. Do you think his/her inference logic is right? Why or why not?
  - c) The sketches below illustrate two common types of pavement surface distresses or damages, what are the most likely causes for each of the damages?



- 6. A flexible pavement has been designed with a 4-in. hot-mix asphalt concrete wearing surface and a 12-in. soil cement base (no subbase). The following data have been used in the design:
  - The annual daily volume in the first year is expected to be 300 trucks per lane. Each truck has two 16-kip single axles.
  - The overall standard deviation is 0.40, the drainage coefficients are set as 1.0 and the subgrade resilient modulus is 5000 psi.
  - Terminal PSI = 2.0 and initial PSI = 4.5.
  - a) If the truck volume will increase at an annual rate of 5% during the first 5 years and will then remain the same for the rest years, how long will the pavement last at the level of confidence of 90%?
  - b) Give three examples on how pavement quality and performance can be measured?

[You can use either Design Equation or Design Chart]

- a). A vertical curve is designed to provide safe stopping sight distance. The PVC of the curve is at station 1+ 234.000 with elevation of 1100 m while the PVI is at station 1+ 324.000 (elevation 1100 m). The elevation at PVT is 1102.00 m. Based on the AASHTO design standard, is the curve adequate for a design speed of 100 km/h? Why or why not?
  - b). You are asked to locate a directional sign near the exit of a freeway ramp. How far should the directional sign be placed ahead of the exit of the freeway ramp? The following information is available for your analysis:
    - The freeway has a posted speed of 120 km/h and the posted ramp speed is 30 km/h;
    - Past research experiments indicated that most drivers can read a traffic sign within his or her area of vision at a distance of 50 meters when traveling at a speed of 120 km/h, and need 1 second to complete their reading and 1 second to decide and react (i.e., press brake to slow down if they want to exit);
    - The highway section is on a 2% downgrade with a coefficient of road adhesion of 0.60 and a coefficient of friction of 0.28.

# **Equations**

#### Geometric Design

$$SSD = V_0^2/[2g(f+G)] + V_0 t_{pr}$$
 
$$d = (V_0^2 - V_t^2)/[2g(f+G)] + V_0 t_{pr}$$

#### Horizontal:

$$\begin{split} R_v &= V^2/[g \ (f_s + e)] \\ T &= R \ tan \ (\Delta/2); \ L = \pi \ \Delta \, R \, / \, 180 \ ; \ M = R - R \cos(\Delta/2); \ E = R \, / \cos(\Delta/2) - R \\ \Delta_s &= 2 \cos^{-1} \left( 1 - M_s / R_v \right) \\ M_s &= R_v - R_v \cos \left[ (90 \ SSD) / (\pi \ R_v) \right] \end{split}$$

#### Vertical:

$$y = (G_2 - G_1)/(2L) \quad x^2 + G_1 \quad x \; ; \; Y = A \quad x^2 / (200L)$$

$$S = L/2 + 100(\sqrt{H_1} + \sqrt{H_2})^2 / A \quad \text{or} \quad L = 2S - 200 \left(\sqrt{H_1} + \sqrt{H_2}\right)^2 / A \quad (S \ge L)$$

$$S = \sqrt{\frac{200L}{A}} \left(\sqrt{H_1} + \sqrt{H_2}\right) \quad \text{or} \quad L = \frac{A S^2}{200(\sqrt{H_1} + H_2)^2} \quad (S < L)$$

$$S = \frac{A L + 200H}{2A - 200 \tan \beta} \quad \text{or} \quad L = 2S - 200(H + S \tan \beta) / A \quad (S \ge L)$$

$$S = \frac{100L \tan \beta + \sqrt{(100L \tan \beta)^2 + 200ALH}}{A} \quad \text{or} \quad L = \frac{A S^2}{200(H + S \tan \beta)}$$
 (S

$$L_m = K A \text{ where } K = SSD^2 / 658$$
  
 $L_m = K A \text{ where } K = SSD^2 / (120+3.5 SSD)$ 

#### Pavement Design (Flexible)

Traffic Growth Factor (TGF) =  $[(1+r)^n - 1]/r$  where r = growth rate Design ESAL's = TGF \* Present Daily ESAL \* 365 SN =  $a_1$  D<sub>1</sub> +  $a_2$  D<sub>2</sub> M<sub>2</sub> +  $a_3$  D<sub>3</sub> M<sub>3</sub>

$$\log_{10}(W_{18}) = Z_{R} \times S_{o} + 9.36 \times \log_{10}(SN+1) - 0.20 + \frac{\log_{10}(\frac{\Delta PSI}{4.2-1.5})}{0.40 + \frac{1094}{(SN+1)^{5.19}}} + 2.32 \times \log_{10}(M_{R}) - 8.07$$

# **Tables**

#### 1) Coefficient of friction and coefficient of side friction

| Initial Vehicle<br>Speed (km/h) | Coefficient of Friction (f) | Coefficient of Side Friction (fs) |  |  |
|---------------------------------|-----------------------------|-----------------------------------|--|--|
| 30                              | 0.40                        | 0.17                              |  |  |
| 40                              | 0.38                        | 0.17                              |  |  |
| 50                              | 0.35                        | 0.16                              |  |  |
| 60                              | 0.33                        | 0.15                              |  |  |
| 70                              | 0.31                        | 0.14                              |  |  |
| 80                              | 0.30                        | 0.14                              |  |  |
| 90                              | 0.30                        | 0.13                              |  |  |
| 100                             | 0.29                        | 0.12                              |  |  |
| 110                             | 0.28                        | 0.11                              |  |  |
| 120                             | 0.28                        | 0.09                              |  |  |

#### 2) Z-statistics table

**Table 4.5** Cumulative Percent Probabilities of Reliability, R, of the S Corresponding  $Z_R$ 

| R  | 0      | 1      | 2      | 3      | 4      | 5      | 6      |
|----|--------|--------|--------|--------|--------|--------|--------|
| 90 | 1.282  | -1.341 | -1.405 |        |        |        | -1.751 |
| 80 | -0.842 | -0.878 | ():915 | -0.954 | _0.994 | =1.036 | _1 080 |

## 3) Structural layer coefficients

| Pavement component            | Coefficient |  |
|-------------------------------|-------------|--|
| Wearing surface               |             |  |
| Sand-mix asphaltic concrete   | 0.35        |  |
| Hot-mix asphaltic concrete    | ().44       |  |
| Base                          |             |  |
| Crushed stone                 | 0.14        |  |
| Dense-graded crushed stone    | 0.18        |  |
| Soil cement                   | 0.20        |  |
| Emulsion/aggregate-bituminous | 0.30        |  |
| Portland cement/aggregate     | 0.40        |  |
| Lime-pozzolan/aggregate       | 0.40        |  |
| Hot-mix asphaltic concrete    | 0.40        |  |
| Subbase                       |             |  |
| Crushed stone                 | 0.11        |  |

## 4) LEF

Table 4.2 Axle-Load Equivalency Factors for Flexible Pavements, Single A:

|         |                    |        |        | The same of the sa |  |
|---------|--------------------|--------|--------|--|--|
| l numbe | Pavement structura |        |        | Axle   |  |
|         | 3                  | 2      | 1      | load<br>(kips)   |  |
| 0.      | 0.0003             | 0.0004 | 0.0004 | 2  |  |
| 0.      | 0.004              | 0.004  | 0.003  | 4  |  |
| 0.      | 0.017              | 0.017  | 0.011  | 6  |  |
| 0.      | 0.051              | 0.047  | 0.032  | 8  |  |
| 0.      | 0.118              | 0.102  | 0.078  | 10   |  |
| 0.      | 0.229              | 0.198  | 0.168  | 12   |  |
| 0.      | 0.399              | 0.358  | 0.328  | 14   |  |
| 0.      | 0.646              | 0.613  | 0.591  | 16   |  |
| 1.      | 1.00               | 1.00   | 1.00   | 18   |  |
| 1.      | 1.49               | 1.57   | 1.61   | 20   |  |
| 2.      | 2.17               | 2.38   | 2.48   | 22   |  |
| 2.      | 3.09               | 3.49   | 3.69   | 24   |  |
| 3.      | 4.31               | 4.99   | 5.33   | 26   |  |
| 5.      | 5.90               | 6.98   | 7.49   | 28   |  |
| 6.      | 7.9                | 9.5    | 10.3   | 30   |  |
|         |                    |        |        |  |  |

Table 4.1. Axis Load Equivalency Lactors for Flexible Pavements, Tandem Axiss, and TS1 = 2.5

| 1.16            | Pavement structural number (SN) |                |        |            |        |        |  |
|-----------------|---------------------------------|----------------|--------|------------|--------|--------|--|
| logid<br>(kipsa | 1                               | 20             | 3      | <i>e</i> } | 5      | 6      |  |
|                 | 0 (00)1                         | 0.0001         | 0.0001 | 0.0000     | 0.0000 | 0,0000 |  |
| i i             | 0.0005                          | 7(000)         | 0.0004 | 0.0003     | 0.0003 | 0.0002 |  |
| 0               | 0.003                           | 0.002          | 0.002  | 0,001      | 0.001  | 0.001  |  |
| 5               | 0.001                           | 0.006          | 0,005  | 0.004      | 0.003  | 0.003  |  |
| .0              | 0.008                           | 0.013          | 0.011  | 0.009      | 0.007  | 0.006  |  |
| 2               | 0.012                           | (E(),\dagger_4 | 0.023  | 0.018      | 0.014  | 0.013  |  |
| 1               | 0,056                           | 0.041          | 0.042  | 0.033      | 0.027  | 0.024  |  |
| ń               | 0.04                            | 0.065          | 0.070  | 0.057      | 0.047  | 0.043  |  |
| Ь               | 0.070                           | 0.097          | 0.109  | 0.092      | 0.077  | 0.070  |  |
| ()              | 0.107                           | 0 (4)          | 0,162  | 0.141      | 0.121  | 0.110  |  |
|                 | 0.160                           | 0.198          | 0,229  | 0,207      | 0.180  | 0.166  |  |
| 4               | 0.231                           | 0.273          | 0.315  | 0.292      | 0.260  | 0.242  |  |
| (s              | 0.127                           | 0,120          | 0,420  | 0.401      | 0.364  | 0,342  |  |
| 5               | 0.431                           | 0,493          | 0,548  | 0.534      | 0.495  | 0.470  |  |
| (1)             | 0.611                           | 0.648          | 0.703  | 0.695      | 0.658  | 0.633  |  |
| ,               | 118.0                           | 0.843          | 0,889  | 0.887      | 0.857  | 0.834  |  |
|                 | 1.06                            | 1.08           | 1,11   | 1.11       | 1.09   | 1,08   |  |
| 6               | 1.38                            | 1.38           | 1,38   | 1.38       | 1.38   | 1.38   |  |
| S               | 1.75                            | 1.73           | 1.69   | 1.68       | 1.70   | 1.73   |  |
| ()              | 2,24                            | 2.16           | 2,06   | 2.03       | 2.08   | 2.14   |  |
| 2               | 1 16                            | 2,67           | 2,49   | 2.43       | 2.51   | 2.61   |  |
| 4               | 3.41                            | 1,27           | 2.99   | 2.88       | 3.00   | 3.16   |  |
| (1              | 4.18                            | 1.98           | 3,58   | 3,40       | 3,55   | 3.79   |  |
| B               | 5.08                            | 4.80           | 4.25   | 3.98       | 4,17   | 4.49   |  |
| 0               | 6.12                            | 5,76           | 5,03   | 4.64       | 4.86   | 5.28   |  |
| )               | 7.,1.1                          | 6.87           | 5.93   | 5,38       | 5,63   | 6.17   |  |
| .               | 8,72                            | 8,14           | 6.93   | 6.22       | 6.47   | 7.15   |  |
| ()              | 10.3                            | 9,6            | 8.1 -  | 7.2        | 7.4    | 8.2    |  |
| K               | 12-1                            | 11.3           | 9,4    | 8.2        | 8.4    | 9.4    |  |
| 0               | 14.2                            | 13,1           | 10,9   | 9.4        | 9.6    | 10.7   |  |
| 2               | 16.5                            | 15.3           | 12.6   | 10.7       | 10.8   | 12.1   |  |
| i               | 19,1                            | 17,6           | 14,5   | 12.2       | 12.2   | 13.7   |  |
| 6               | 22,1                            | 20.3           | 16,6   | 13,8       | 13.7   | 15.4   |  |
| ĸ               | 25.3                            | 23.3           | 18.9   | 15.6       | 15.4   | 17.2   |  |
| 0               | 29,0                            | 26,6           | 21.5   | 17.6       | 17.2   | 19.2   |  |
| 3               | 33.0                            | 30,3           | 24.4   | 19,8       | 19.2   | 21.3   |  |
|                 | 37.5                            | 34,4           | 27.6   | 22.2       | 21.3   | 23.6   |  |
| h               | 42.5                            | 38.9           | 31.1   | 24.8       | 23.7   | 26.1   |  |
| В               | 48.0                            | 43.9           | 35,0   | 27.8       | 26.2   | 28.8   |  |
| ()              | 54.0                            | 49.4           | 39.2   | 30.9       | 29.0   | 31.7   |  |
| 2               | 60,6                            | 55.4           | 43.9   | 34.4       | 32.0   | 34.8   |  |
| 4               | 67.8                            | 61,9           | 49.0   | 38.2       | 35.3   | 38.1   |  |
| 6               | 75.7                            | 69.1           | 54.5   | 42.3       | 38.8   | 41.7   |  |
| 8               | 84.3                            | 76.9           | 60.6   | 46.8       | 42,6   | 45.6   |  |
| 0               | 93.7                            | 85.4           | 67.1   | 51.7       | 46.8   | 49.7   |  |

Source: AASHTO Guide for Design of Pavement Structures, The American Association of State Highway and Transportation Officials, Washington, DC, 1993. Used by permission.

# **Design Equation and Chart for Flexible Pavement**

