

NATIONAL EXAMINATIONS

May 2014

07-MEC-B3 ENERGY CONVERSION AND POWER GENERATION

Three hours duration

Notes to Candidates

1. This is a **Closed Book** examination.
2. Examination paper consists of two Sections. **Section A is Calculative** with four (4) questions and **Section B is Descriptive** with two (2) questions.
3. Note that Question 4 and Question 5 are each on two pages.
3. **Do three (3) questions (including all parts of each question) from Section A (Calculative) and one (1) question from Section B (Descriptive).**
4. **Four questions constitute a complete paper. (Total 60 marks).**
5. **All questions are of equal value. (Each 15 marks).**
6. If doubt exists as to the interpretation of any question or in the event of missing data, the candidate is urged to submit, with the answer paper, a clear statement of any assumptions made.
7. Candidates may use one of the approved **Casio** or **Sharp** calculators.
8. **Reference data for particular questions are given on pages 10 to 17. All pages used are to be returned with the answer booklet showing where data has been obtained.**
9. **Reference formulae and constants are given on pages 18 to 21.**
10. **Steam Tables** from "Thermodynamics and Heat Power" are provided.

SECTION A CALCULATIVE SECTION

QUESTION 1 STEAM PLANT DESIGN

Consider the proposed construction of a new coal fired power plant where an estimate of the required resources (fuel and water) and costs are required. The basic parameters are as follows:

Capacity of power plant	500 MW
Capacity factor of plant*	0.80
Life expectancy of plant	40 years
Heat rate of whole plant**	10 550 kJ/kWh
Efficiency of boiler	90%
Capital cost of plant	2 500 \$/kW
Cost of capital repayments	10% of capital cost each year
Cost of administration and maintenance	8% of capital cost each year
Cost of coal	100 \$/Mg
Heating value of coal	24 000 kJ/kg
Capacity of one train car	50 Mg
Number of coal cars per train	60

Note: *Capacity factor = actual electrical output / maximum possible electrical output

**Heat rate is inverse of thermal efficiency

Determine the following for a cooling water temperature rise of 10°C:

- (a) Annual actual electrical production (kWh) and maximum possible electrical production (kWh).
- (b) Annual amount of coal required (Mg) and number of trains required per day.
- (c) Annual cost of coal (\$) and cost of coal per unit generated (cent/kWh).
- (d) Annual capital cost repayment (\$) and cost per unit generated (cent/kWh).
- (e) Annual administration and maintenance cost (\$) and cost per unit generated (cent/kWh).
- (f) Total power production cost per unit generated (cent/kWh).
- (g) Rate of heat rejection in cooling water from steam cycle at full load (kJ/s).
- (h) Quantity of cooling water required at full load (m^3/s).

[15 marks]

QUESTION 2 STEAM INJECTED GAS TURBINE

Refer to the Examination Paper Attachments Page 10 Steam Injected Gas Turbine

A steam injected gas turbine system, as shown in the attachment, consists of an air compressor, a combustion chamber, a gas turbine, a once through heat recovery steam generator and a feedwater pump. Both the gas and steam systems are open cycles. The gas turbine can operate with or without steam injection. The operational parameters with steam injection are as follows:

Gas cycle pressure ratio	= 12
Air compressor air inlet temperature	= 30°C
Gas turbine gas inlet temperature	= 1000°C (without steam)
Steam generator steam outlet pressure	= 1.2 MPa
Steam generator steam outlet temperature	= 300°C
Steam generator water inlet temperature	= 30°C
Steam generator gas outlet temperature	= 160°C
Steam turbine exhaust pressure	= 0.1 MPa
Air compressor efficiency	= 0.80
Gas turbine efficiency	= 0.90 (with gas)
Gas turbine efficiency	= 0.90 (with steam)
Feedwater pump efficiency	= 1.00
Electrical generator efficiency	= 1.00
Fuel calorific value	= 42 000 kJ/kg

Assume cold air standard cycle (constant specific heats with $k = 1.4$). For a gas mass flow of 100 kg/s calculate the following but see note below for acceptable assumptions:

- (a) Mass flow rate of fuel (kg/s).
- (b) Mass flow rate of steam (kg/s) during injection.
- (c) Power output with steam injection (MW).
- (d) Cycle efficiency with steam injection.

Note: Consider the gas and steam flows through the gas turbine and heat exchanger as separate streams with different properties and temperatures neglecting the transfer of heat between the two streams. It is not necessary to iterate to obtain more accurate answers. Use the point identifying numbers as shown on the accompanying diagram. For the thermodynamic calculations assume that the steam is injected at the place indicated.

[15 marks]

QUESTION 3 STEAM TURBINE OPERATIONAL CONDITIONS

Refer to the Examination Paper Attachments Page 11 Mollier Chart.

Steam is supplied to a turbine with an internal efficiency of 80% at 4 MPa (40 bar) and 400°C and exhausts at 0.005 MPa (0.05 bar). At full load the steam flow is 24 kg/s.

Note that the Mollier Chart is in bar (1 bar = 0.1 MPa).

Note that the steam flow under part load conditions is proportional to the inlet turbine pressure. Assume that for parts (a) to (c) the exhaust pressure remains constant.

- (a) Calculate the power developed by the turbine at full load.
- (b) Calculate the power developed by the turbine when the inlet steam is throttled to 1 MPa. Assume that the internal efficiency is unchanged.
- (c) Calculate the power developed by the turbine when the generator output is zero. Under these conditions the turbine power output is dissipated in friction in the bearings and windage in the generator. An inlet steam pressure of 0.1 MPa is required to maintain this condition. Assume that the internal efficiency has decreased to 70%.

Plot the processes on the Mollier Diagram on Page 11 but use Steam Tables to obtain improved accuracy in the calculations if necessary.

Return this page with the examination answer booklet.

Refer to the Examination Paper Attachments Page 12 Condenser Conditions. This shows the temperature profile in the condenser at full load. Assume now that the exhaust temperature does change with load and that the inlet cooling water temperature remains constant.

- (d) Using average temperature differences (not log mean) determine the temperature profiles for steam and water at part load conditions as defined in (b) above and plot these on the diagram.
- (e) Determine the condenser pressure at the temperature determined in (b) above.
- (f) Estimate (without further calculation) the condenser pressure for zero load conditions as defined in (c) above.

Return this page with the examination answer booklet.

[15 marks]

QUESTION 4 WIND AND WATER POWER

PART I WIND TURBINE

Refer to the Examination Paper Attachments Page 13 **Vestas Wind Turbine** and Page 14 **Wind Power Efficiencies**.

The tables and graphs give information for the Vestas V80 1.8 MW Wind Turbine, as well as efficiencies, for ideal and actual wind turbines. Determine the following for a wind speed of 10 m/s and compare with the specified output.

- (a) Kinetic energy and potential power available in the wind passing through a flow area equivalent to the area swept out by the rotor at the wind speed given above.
- (b) Maximum theoretical power and efficiency that can be obtained based on energy and momentum theoretical equations for any wind speed.
- (c) Ideal efficiency and power based on ratio of blade tip speed to wind speed as given (from graph of efficiency on page 14).
- (d) Actual efficiency and power based on ratio of blade tip speed to wind speed as given (from graph of efficiency on Page 14).
- (e) Actual power output at the given wind speed as specified by the manufacturer (from graph on page 13).

(5 marks)

Question 4 continued on next page

QUESTION 4 (Continued)**PART II. VAN DER KLOOF HYDRO POWER STATION**

Refer to the Examination Paper Attachments Page 15 **Van der Kloof Hydro Power Station**. This shows a cross-sectional drawing of the plant close to the main wall of the dam. It has the following design parameters:

Reservoir water level	1170.5 m	(point 1)
Turbine inlet elevation	1091.5 m	(point 2)
Turbine outlet elevation	1086.5 m	(point 3)
Tailrace water level	1094.7 m	(point 4)
Penstock (inlet) diameter	7.0 m	(point 2)
Draft Tube (outlet) diameter	5.0 m	(point 3)
Turbine inlet pressure	700 kPa gauge	(point 2)
Turbine outlet pressure	65 kPa gauge	(point 3)
Water volume flow rate	200 m ³ /s	

Calculate the following:

- (a) (i) The water velocity at the turbine inlet (point 2) and at the turbine outlet (point 3).
- (ii) The head loss in the intake pipe (penstock) (between point 1 and point 2) and in the outlet pipe (draft tube) and tailrace (between point 3 and point 4). (5)

- (b) (i) The potential power output of the whole plant based on elevation difference (between point 1 and point 4) and flow.
- (ii) The hydraulic power developed in the turbine based on inlet and outlet conditions (between point 2 and point 3) assuming no losses within the turbine. (5)

(10 marks)

[15 marks]

SECTION B DESCRIPTIVE SECTION

Descriptive questions [parts of Question 5 and all of Question 6] should be answered in essay form with sketches, if appropriate, and taking approximately one full page for every 5 marks. A full page means approximately 250 words unless diagrams take the place of some words.

While each part of each question specifies several aspects, more emphasis may be put on one or more aspects and less on others provided an overall comprehensive answer is given as required by the above.

QUESTION 5 GRAPHICAL REPRESENTATION

PART I T-s DIAGRAMS

Refer to the Examination Paper Attachments Page 16 T-s and p-V Diagrams.

- (a) On the diagrams given draw T-s and p-V Diagrams for the following thermodynamic power cycles:

- (i) Rankine cycle (saturated conditions)
- (ii) Rankine cycle with superheating
- (iii) Rankine cycle with superheating and reheating
- (iv) Brayton cycle
- (v) Otto cycle
- (vi) Diesel cycle

Return this page with the examination answer booklet.

- (c) Explain why T-s diagrams are traditionally used to show certain cycles and p-V diagrams used to show other cycles. Clarify what parameter is the same for both types of diagrams.
- (d) Explain the advantages of superheating and reheating in the Rankine cycle.

(10 marks)

Question 5 continued on next page

QUESTION 5 (Continued)

PART II LOAD SCHEDULING

Refer to the Examination Paper Attachments Page 17 Daily Load Curve. This curve shows the daily power demand on a typical power system with the maximum demand being somewhat less than the total installed capacity of the system.

Consider a power utility having the following types of power generating equipment with their respective capacities given as a percentage of the total installed capacity:

- Fossil fuel plant 30%
- Nuclear plant 30%
- Gas turbines 10%
- Solar energy 5%
- Wind turbines 10%
- Hydro turbines 5%
- Pumped storage hydro 10%

- (a) Show by blocking in under the curve on the diagram when and to what degree these generating units should be operated assuming a normal sunny day with no wind.
- (b) Considering operating costs clarify which generating equipment would be reduced in load if wind power was available.
- (c) Considering operating costs clarify which generating equipment would be increased in load if the peak demand reached 90% of installed capacity.

Return this page with the examination answer booklet.

(5 marks)

[15 marks]

QUESTION 6 ENERGY CONSIDERATIONS

PART I FOSSIL FUEL CHARACTERISTICS

- (a) Explain the difference between the higher heating value (HHV or HCV) and the lower heating value (LHV or LCV) of a fossil fuel.
- (b) With regard to coal state what constitutes a Proximate Analysis and what constitutes an Ultimate Analysis. Clarify the usefulness of each.
- (c) Compare a high grade coal such as anthracite which is nearly pure carbon with natural gas which is primarily methane. State which one will give lower carbon dioxide emissions for the same energy release. Explain in detail what parameters need to be known to quantify this and how it would be proven that one or the other would give reduced emissions.

(10 marks)

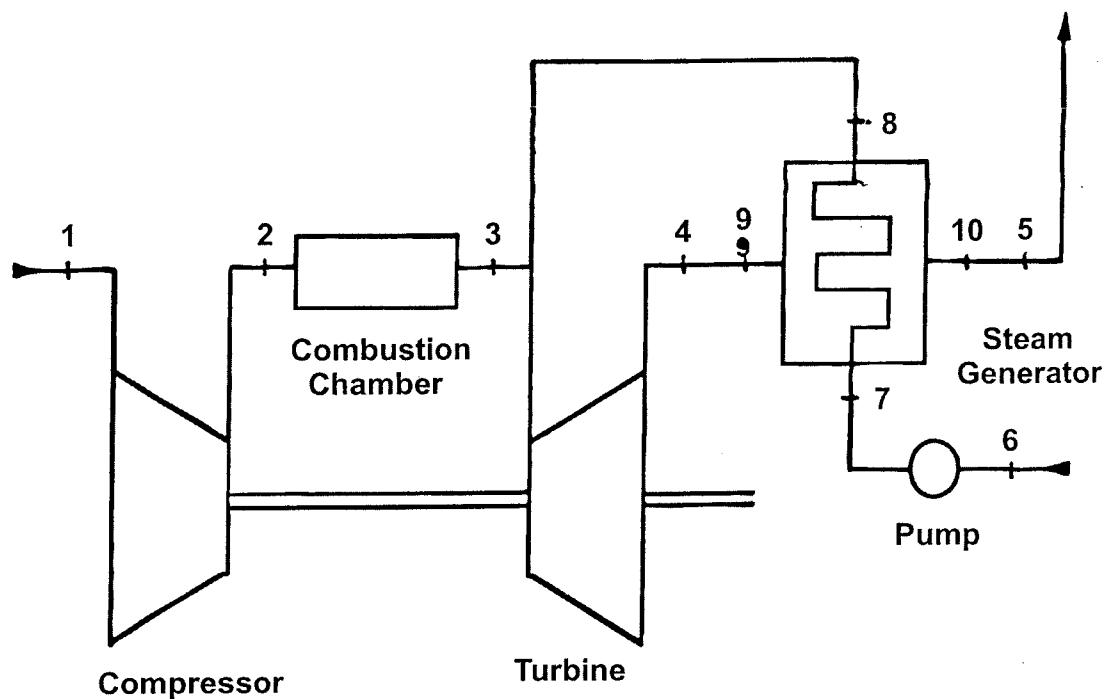
PART II RENEWABLE ENERGY EFFICIENCIES

- (a) Hydro turbines can theoretically convert all (100%) the potential energy in the water into electrical energy but wind turbines can only theoretically convert a little more than half (59%) of the kinetic energy of the wind into electrical energy. Explain why this is the case.
- (b) Solar power plants can only convert part (approximately 20%) of the incoming solar radiation into electrical energy. Compare solar voltaic (solar photovoltaic panels) and solar thermal (reflecting collectors and steam cycle) systems and explain where and why the losses which limit efficiency occur.

(5 marks)

[15 marks]

QUESTION 2 STEAM INJECTED GAS TURBINE

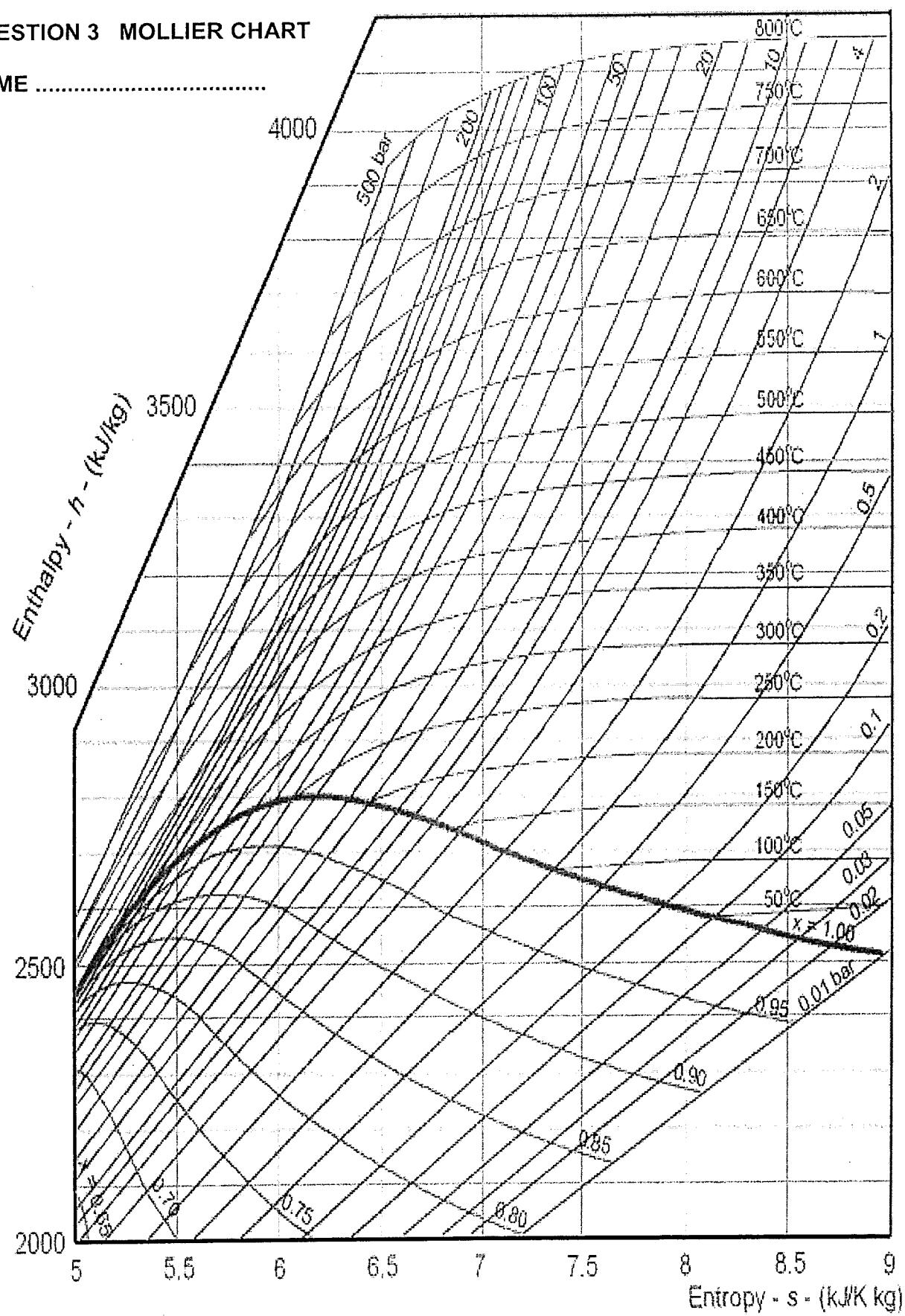


Gas Cycle 1 - 2 - 3 - 4 - 5

Steam Cycle 5 - 7 - 8 - 9 - 10

QUESTION 3 MOLLIER CHART

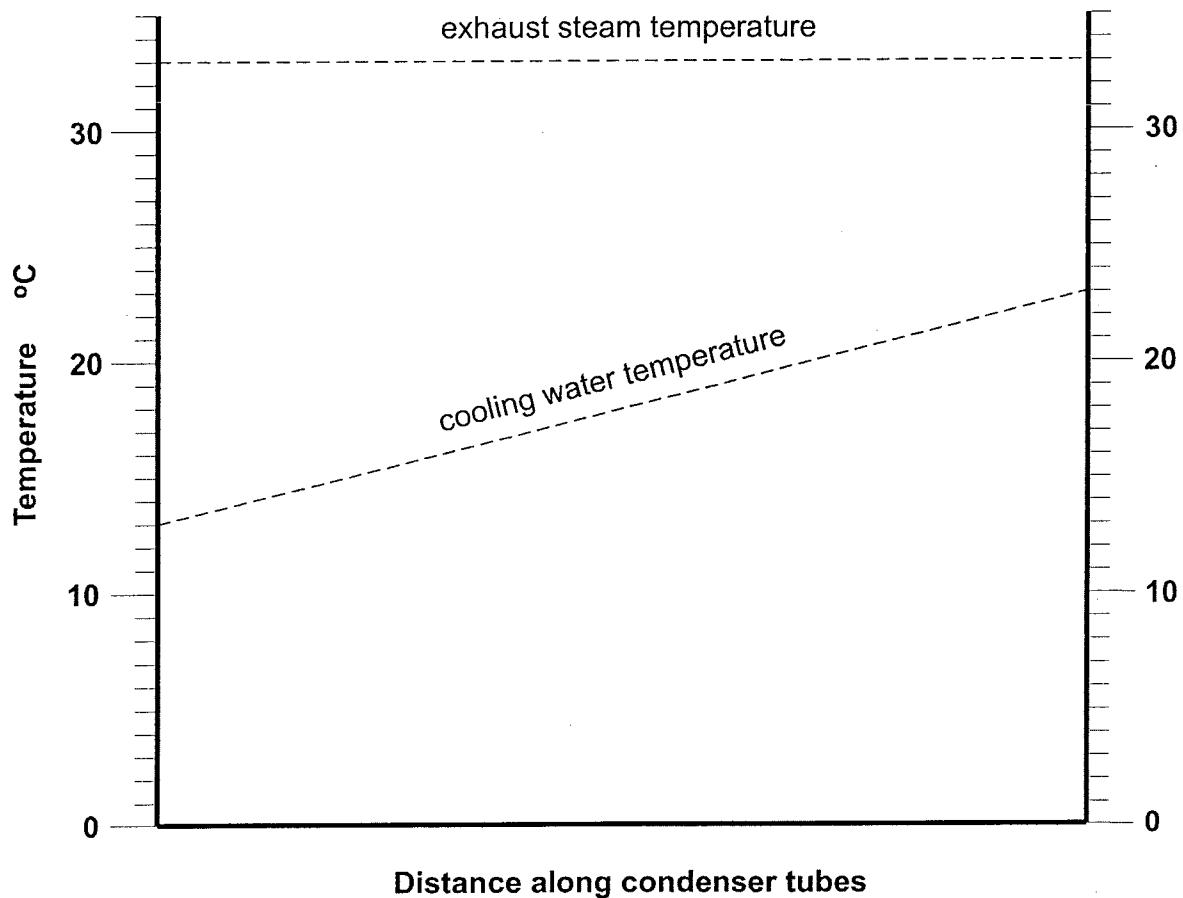
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NAME

QUESTION 3 CONDENSER CONDITIONS

- (d) Show temperature profiles (exhaust steam and cooling water) for part load conditions (when throttled to 4 MPa).
Assume that the cooling water inlet temperature remains constant



- (e) Determine the condenser pressure at part load conditions (4 MPa steam inlet)
- (f) Estimate the exhaust steam temperature and condenser pressure at zero load conditions (0.1 MPa steam inlet)

QUESTION 4 PART I VESTAS WIND TURBINE

**V80 – 1.8 MW**

Pitch regulated wind turbine
with OptiSlip® and OptiTip®

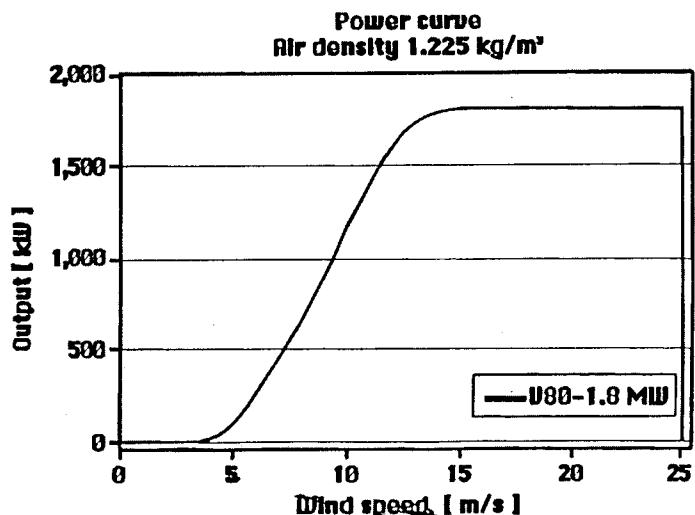
MOTOR	
Diameter:	80 m
Swept area:	5,027 m ²
Speed of revolution:	15.7 RPM
Number of blades:	3
Power regulation:	Pitch + OptiSlip®
Air brake:	3 separate pitch settings
TOWER:	
Hub height (approx.): 60 - 67 - 78 m	
OPERATIONAL DATA:	
Cut-in wind speed:	4 m/s
Nominal wind speed:	16 m/s
Stop wind speed:	25 m/s
GENERATOR:	
Type:	Asynchronous with OptiSlip®
Nominal output:	1.8 MW
Operational data:	60 Hz 690V 1,800 - 1,900 RPM
GEARBOX:	
Type:	Planet/parallel gear
CONTROL:	
Type:	Microprocessor-based control of all turbine functions with the option of remote monitoring. OptiSlip® output regulation and OptiTip® pitch regulation of the blades.
WEIGHT: (APPROX.)	
	(60 m) (67 m) (78 m)
Nacelle:	63 t
Rotor:	38 t

Ideal for moderate wind conditions

The V80-1.8 MW is particularly well suited for installation in areas with moderate to high wind conditions, and thanks to OptiSlip®, the turbine can adapt to wind conditions in almost any location. In this way, Vestas continues to strive for excellence by taking firm steps towards the full exploitation of wind energy.

Advanced Vestas technology

The Vestas V80-1.8 MW is based on the well-known technology from the V66-1.65 MW turbine. The turbine is a three blade 60 Hz pitch-regulated wind turbine with OptiSlip® and OptiTip®. The turbine's rotor diameter is 80 meters – and the turbine can be delivered with tower heights of up to 78 meters.



QUESTION 4 PART I WIND POWER EFFICIENCIES

Wind Power 135

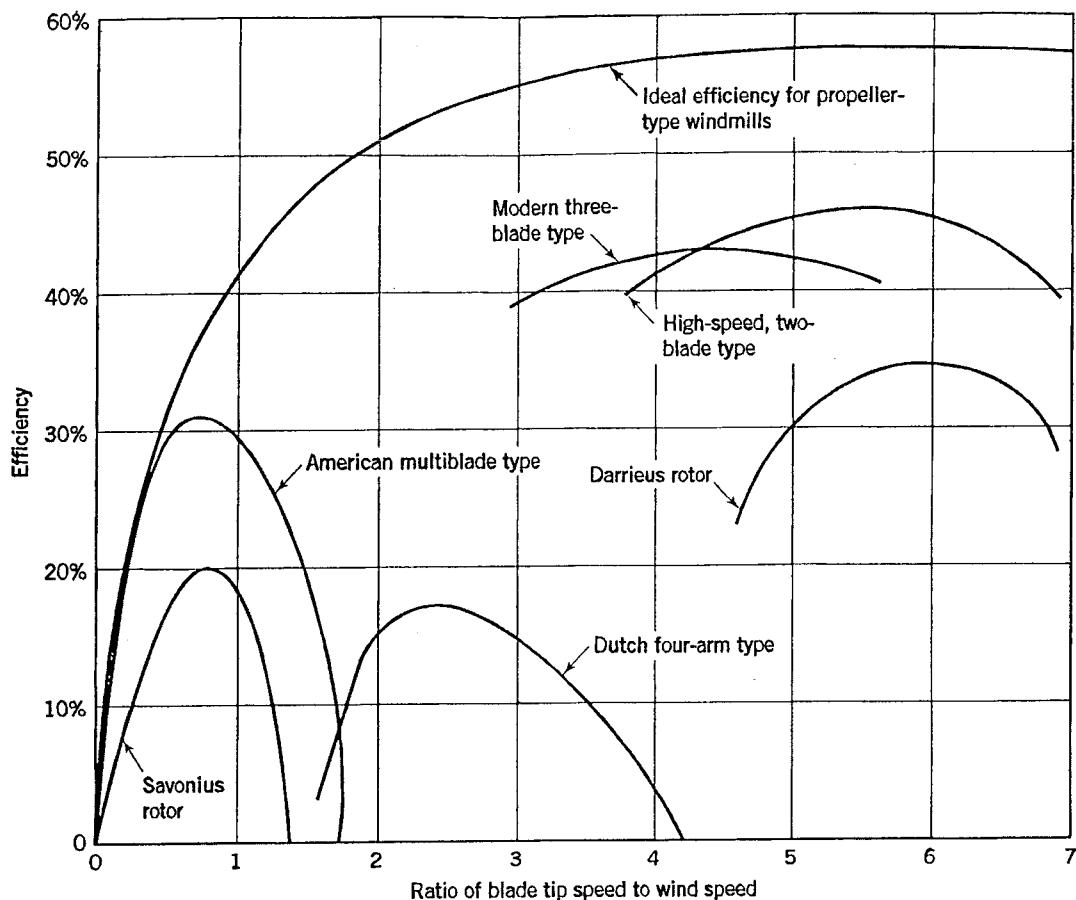


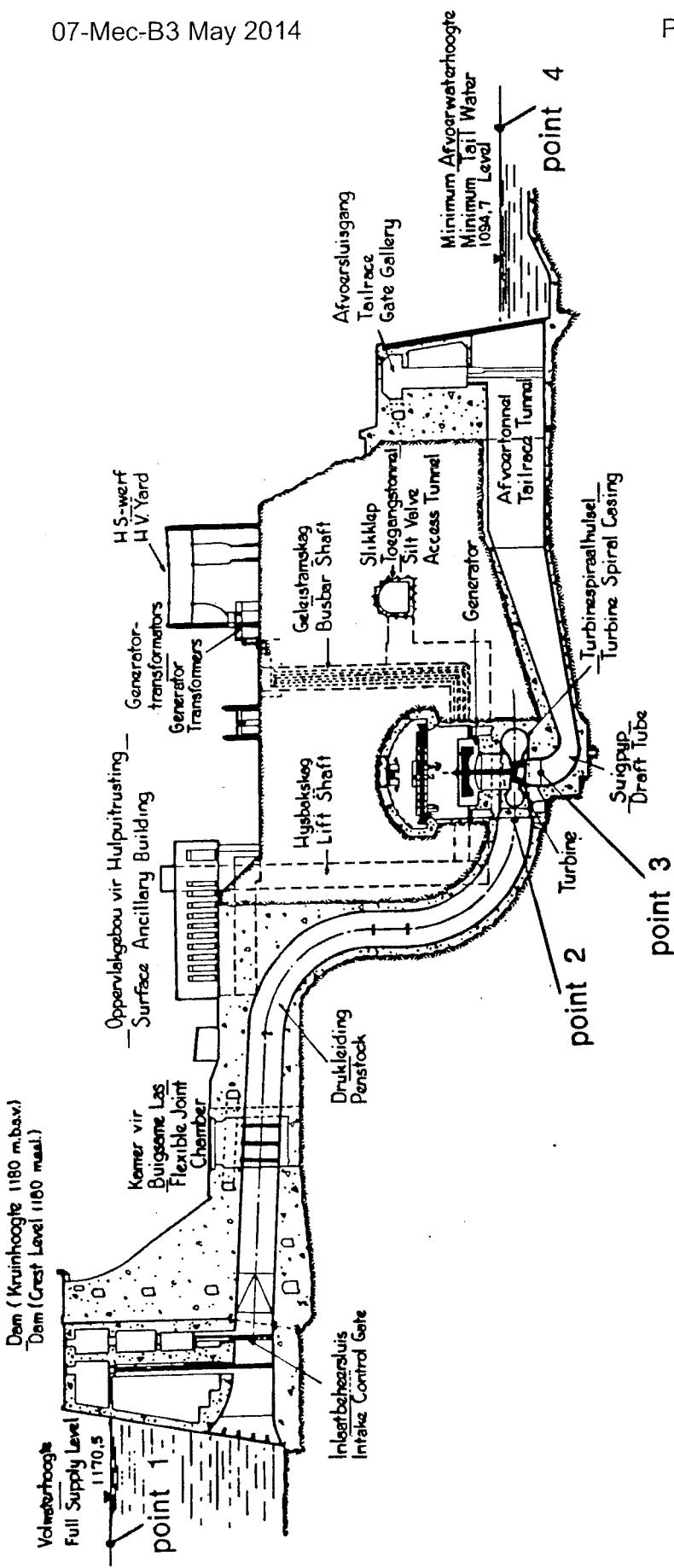
Figure 5.6 Typical efficiencies of several types of windmills plotted against their tip speed ratio. The maximum efficiencies are seen to vary from about 16 to 46%. The ideal efficiency shown is a mathematical ideal, never to be achieved in practice.
 (Source: Basic data from R. Wilson and P. Lissaman, *Applied Aerodynamics of Wind Power Machines*, Oregon State University.)

QUESTION 4 PART II VANDERKLOOF HYDRO POWER STATION

Cross-section through Power Station Waterways/Dwarsdeuruitstroom van Kragstasie-Afvoerkanale

07-Mec-B3 May 2014

Page 15 of 21

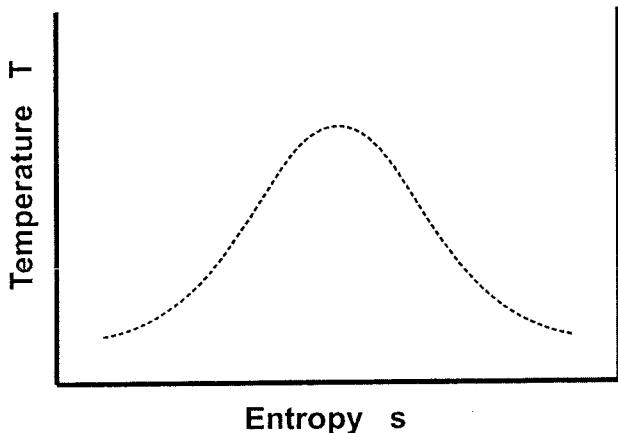


QUESTION 5 PART I T-s DIAGRAMS

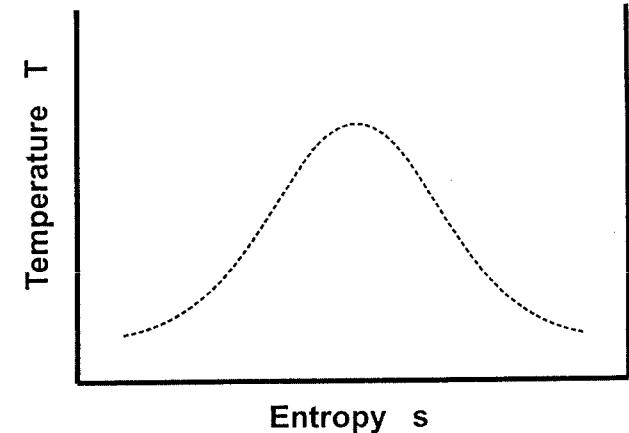
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Draw T-s and p-V diagrams for the cycles specified on the given axes

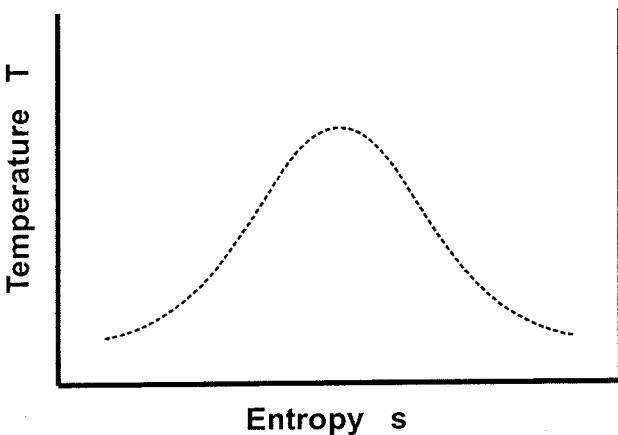
(i) Rankine cycle (saturated conditions)



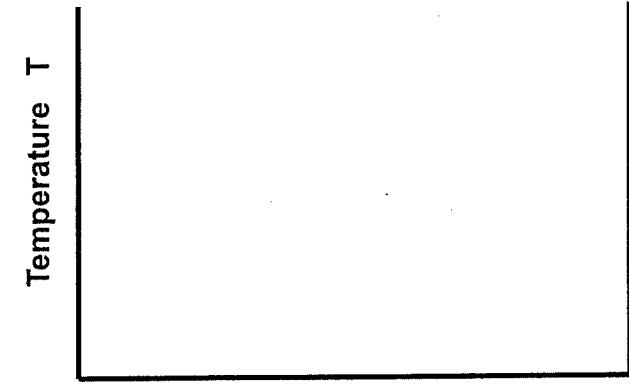
(ii) Rankine cycle with superheat



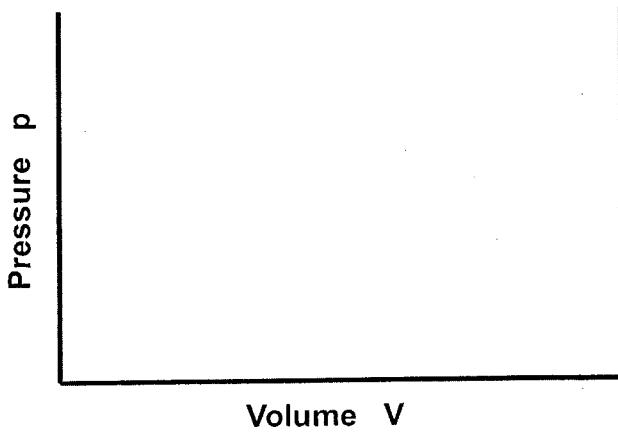
(iii) Rankine cycle with superheat and reheat



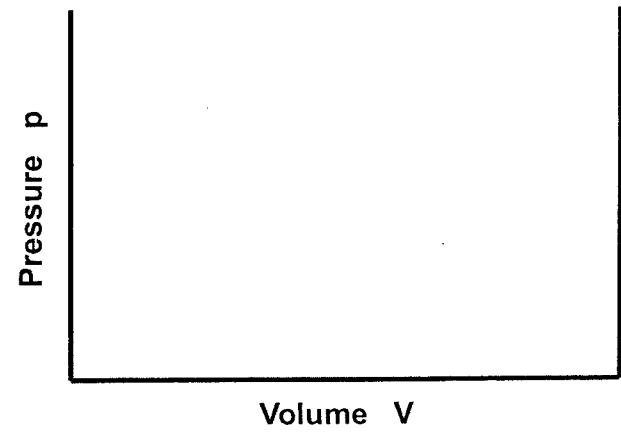
(iv) Brayton cycle



(v) Otto cycle

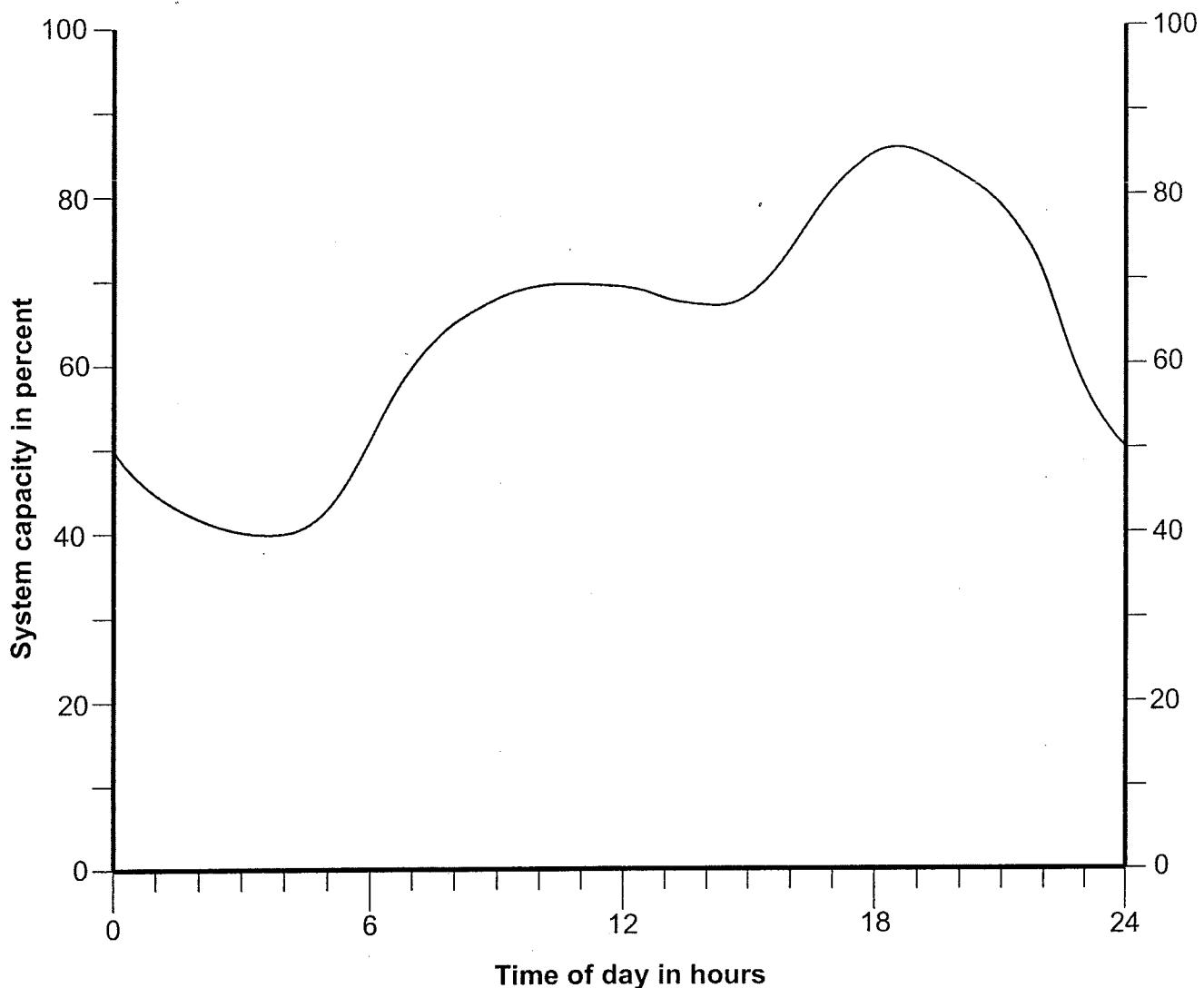


(vi) Diesel cycle

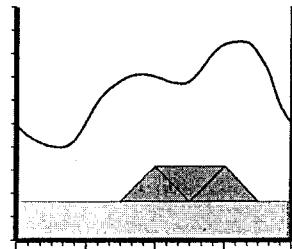


QUESTION 5 PART II DAILY LOAD CURVE

- (a) Show how the given plants would be utilized to meet the daily demand as defined by the curve below



Show the utilization of the various plants by blocking in their output and operational time on the diagram above. The small illustration alongside indicates how this should be done with base load plants at the bottom and peak load plants to make up the remaining demand. Hint: Take account of the fuel price to minimize the overall operational cost



NOMENCLATURE FOR REFERENCE EQUATIONS (SI UNITS)

A	Flow area, Surface area	m^2
c_p	Specific heat at constant pressure	$\text{J/kg}^\circ\text{C}$
c_v	Specific heat at constant volume	$\text{J/kg}^\circ\text{C}$
D	Diameter	m
E	Energy	J
g	Gravitational acceleration	m/s^2
h	Specific enthalpy	J/kg
k	Ratio of specific heats	
L	Length	m
m	Fractional mass flow rate	
m	Mass	kg
M	Mass flow rate	kg/s
p	Pressure	$\text{Pa } (\text{N/m}^2)$
q	Heat transferred	J/kg
Q	Heat	J
Q	Volume flow rate	m^3/s
R	Specific gas constant	J/kg K
s	Entropy	J/kg K
T	Temperature	K
u	Specific internal energy	J/kg
U	Overall heat transfer coefficient	$\text{W/m}^{2\circ}\text{C } (\text{J/sm}^{2\circ}\text{C})$
v	Specific volume	m^3/kg
V	Velocity	m/s
w	Specific work	J/kg
W	Work	J
x	Length	m
z	Elevation	m
η	Efficiency	\circ
θ	Nozzle angle	$^\circ$
$\Delta\theta$	Temperature difference between fluids	$^\circ\text{C}$
μ	Dynamic viscosity	Ns/m^2
ν	Kinematic viscosity	m^2/s
ρ	Density	kg/m^3
T	Thrust	N
Ω	Heat transfer rate	J/s

GENERAL CONSTANTS

Acceleration due to gravity: $g = 9.81 \text{ m/s}^2$	Specific heat of air: $c_p = 1.005 \text{ kJ/kg}^\circ\text{C}$
Atmospheric pressure: $p_{atm} = 100 \text{ kPa}$	Specific heat of air: $c_v = 0.718 \text{ kJ/kg}^\circ\text{C}$
Density of water: $\rho_{water} = 1000 \text{ kg/m}^3$	Specific heat of helium: $c_p = 5.193 \text{ kJ/kg}^\circ\text{C}$
Specific heat of water: $c_p = 4.190 \text{ kJ/kg}^\circ\text{C}$	Specific heat of helium: $c_v = 3.117 \text{ kJ/kg}^\circ\text{C}$

THERMODYNAMICS REFERENCE EQUATIONS

Basic Thermodynamics

First Law:	$dE = \delta Q - \delta W$
Enthalpy:	$h = u + pv$
Continuity:	$\rho VA = \text{constant}$
Flow Work:	$w = \Delta(pv)$
Energy Equation:	$zg + V^2/2 + u + pv + \Delta w + \Delta q = \text{constant}$
Entropy:	$\Delta s = \Sigma \delta q / T$ (reversible conditions)

Ideal Gas Relationships

Gas Law:	$pv = RT$
Specific Heat at Constant Pressure:	$c_p = \Delta h / \Delta T$
Specific Heat at Constant Volume:	$c_v = \Delta u / \Delta T$
Gas Constant:	$R = c_p - c_v$
Specific Heat Ratio:	$k = c_p / c_v$
Isentropic Relations:	$p_1 / p_2 = (v_2 / v_1)^k = (T_1 / T_2)^{k/(k-1)}$

FLUID MECHANICS REFERENCE EQUATIONS

Fluid Mechanics

- Continuity Equation: $\rho_1 V_1 A_1 = \rho_2 V_2 A_2 = M$
- Bernoulli's Equation: $p_1/\rho g + z_1 + V_1^2/2g = p_2/\rho g + z_2 + V_2^2/2g$
- Momentum Equation: $F = p_1 A_1 - p_2 A_2 - \rho V A (V_2 - V_1)$ (one dimensional)

Steam Turbines

- Nozzle Equation: $h_1 - h_2 = (V_2^2 - V_1^2) / 2$
- Work: $w = [(V_1^2_{\text{absolute}} - V_2^2_{\text{absolute}}) + (V_2^2_{\text{relative}} - V_1^2_{\text{relative}})] / 2$

Gas Turbines

- State Equation: $pv = RT$
- Isentropic Equation: $(T_2/T_1) = (p_2/p_1)^{(k-1)/k}$
- Enthalpy Change: $h_1 - h_2 = c_p(T_1 - T_2)$ (ideal gas)
- Nozzle Equation: $h_1 - h_2 = (V_2^2 - V_1^2) / 2$

Jet Propulsion

- Thrust: $T = M(V_{\text{jet}} - V_{\text{aircraft}})$
- Thrust Power: $T V_{\text{aircraft}} = M(V_{\text{jet}} - V_{\text{aircraft}}) V_{\text{aircraft}}$
- Jet Power: $P = M(V_{\text{jet}}^2 - V_{\text{aircraft}}^2) / 2$
- Propulsion Efficiency: $\eta_p = 2V_{\text{aircraft}} / (V_{\text{jet}} + V_{\text{aircraft}})$

Wind Turbine

- Maximum Ideal Power: $P_{\max} = 8 \rho A V_1^3 / 27$

HEAT EXCHANGER REFERENCE EQUATIONS

Heat transferred between fluids

$$\Omega = U A \theta$$

Heat gained or lost by fluids

$$\Omega = M \Delta h$$

$$\Omega = M c_p \Delta T$$

$$\Omega = \rho Q \Delta T$$

NUCLEAR REFERENCE EQUATIONS

Number of nuclei per gram of material

$$N = N_A / M$$

Number of fissile nuclei per cm³ of material

$$N_f = \gamma (N_A / M) \rho$$

Heat release rate in nuclear fuel

$$q^* = \phi N_f \sigma_f E_f$$

Nomenclature

N	=	number of nuclei (number/g)
N_A	=	Avogadro's Number
M	=	molecular weight
γ	=	fuel enrichment
ρ	=	density (g/cm ³)
q^*	=	heat release rate (J/cm ³)
ϕ	=	neutron flux (neutrons/cm ² s)
N_f	=	number of fissile nuclei (number/cm ³)
σ_f	=	cross section (barn) (1 barn = 10 ⁻²⁴ cm ²)
E_f	=	energy release per fission of one atom

Avogadro's Number

$$N_A = 0.602 \times 10^{24} \text{ atoms/mole}$$

Thermodynamics and Heat Power

SIXTH EDITION

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PRENTICE HALL

Upper Saddle River, New Jersey Columbus, Ohio

TABLE A.1 (SI)
Saturation Temperature (Steam)

Temp. °C <i>T</i>	Press. kPa <i>P</i>	Specific Volume (m ³ /kg)			Internal Energy (kJ/kg)			Enthalpy (kJ/kg)			Entropy (kJ/kg · °K)		
		Sat. Liquid <i>v_f</i>	Sat. Vapor <i>v_g</i>	Sat. Liquid <i>u_f</i>	Sat. Vapor <i>u_g</i>	Sat. Liquid <i>h_f</i>	Sat. Vapor <i>h_g</i>	Sat. Liquid <i>s_f</i>	Sat. Vapor <i>s_g</i>	Sat. Liquid <i>s_{f,g}</i>	Sat. Vapor <i>s_{f,g}</i>		
0.01	0.6113	0.001 000	206.14	.00	2375.3	2375.3	.01	2501.3	2501.4	.0000	9.1562	9.1562	
5	0.8721	0.001 000	147.12	20.97	2361.3	2382.3	20.98	2489.6	2510.6	.0761	8.9496	9.0257	
10	1.2276	0.001 000	106.38	42.00	2347.2	2389.2	42.01	2477.7	2519.8	.1510	8.7498	8.9008	
15	1.7051	0.001 001	77.93	62.99	2333.1	2396.1	62.99	2465.9	2528.9	.2245	8.5569	8.7814	
20	2.339	0.001 002	57.79	83.95	2319.0	2402.9	83.96	2454.1	2538.1	.2966	8.3706	8.6672	
25	3.169	0.001 003	43.36	104.88	2304.9	2409.8	104.89	2442.3	2547.2	.3674	8.1905	8.5580	
30	4.246	0.001 004	32.89	125.78	2290.8	2416.6	125.79	2430.5	2556.3	.4369	8.0164	8.4533	
35	5.628	0.001 006	25.22	146.67	2276.7	2493.4	146.68	2418.6	2565.3	.5053	7.8478	8.3531	
40	7.384	0.001 008	19.52	167.56	2262.6	2430.1	167.57	2406.7	2574.3	.5725	7.6845	8.2570	
45	9.593	0.001 010	15.26	188.44	2248.4	2436.8	188.45	2394.8	2583.2	.6387	7.5261	8.1648	
50	12.349	0.001 012	12.03	209.32	2234.2	2443.5	209.33	2382.7	2592.1	.7038	7.3725	8.0763	
55	15.758	0.001 015	9.568	230.21	2219.9	2450.1	230.23	2370.7	2600.9	.7679	7.2234	7.9913	
60	19.940	0.001 017	7.671	251.11	2205.5	2456.6	251.13	2358.5	2609.6	.8312	7.0784	7.9096	
65	25.03	0.001 020	6.197	272.02	2191.1	2463.1	272.06	2346.2	2618.3	.8935	6.9375	7.8310	
70	31.19	0.001 023	5.042	292.95	2176.6	2469.6	292.98	2333.8	2626.8	.9549	6.8004	7.7553	
75	38.58	0.001 026	4.131	313.90	2162.0	2475.9	313.93	2321.4	2635.3	1.0155	6.6669	7.6824	
80	47.39	0.001 029	3.407	334.86	2147.4	2482.2	334.91	2308.8	2643.7	1.0753	6.5369	7.6122	
85	57.83	0.001 033	2.828	355.84	2132.6	2488.4	355.90	2296.0	2651.9	1.1343	6.4102	7.5445	
90	70.14	0.001 036	2.361	376.85	2117.7	2494.5	376.92	2283.2	2660.1	1.1925	6.2866	7.4791	
95	84.55	0.001 040	1.982	397.88	2102.7	2500.6	397.96	2270.2	2668.1	1.2500	6.1659	7.4159	

TABLE A.1 (SI) (cont'd.)

Temp. °C <i>T</i>	Press. kPa <i>P</i>	Specific Volume (m³/kg)				Internal Energy (kJ/kg)				Enthalpy (kJ/kg)		Entropy (kJ/kg · K)	
		Sat. Liquid <i>u_l</i>	Sat. Vapor <i>u_g</i>	Sat. Liquid <i>u_f</i>	Sat. Vapor <i>u_{fg}</i>	Sat. Liquid <i>h_f</i>	Sat. Vapor <i>h_{fg}</i>	Sat. Liquid <i>h_f</i>	Sat. Vapor <i>h_{fg}</i>	Sat. Liquid <i>s_f</i>	Sat. Vapor <i>s_{fg}</i>	Sat. Vapor <i>s_g</i>	
100	0.10135	0.001044	1.6729	418.94	2087.6	2506.5	419.04	2257.0	2676.1	1.3069	6.0480	7.3549	
105	0.12082	0.001048	1.4194	440.02	2072.3	2512.4	440.15	2243.7	2683.8	1.3630	5.9328	7.2958	
110	0.14327	0.001052	1.2102	461.14	2057.0	2518.1	461.30	2230.2	2691.5	1.4185	5.8202	7.2387	
115	0.16906	0.001056	1.0366	482.30	2041.4	2523.7	482.48	2216.5	2699.0	1.4734	5.7100	7.1833	
120	0.19853	0.001060	0.8919	503.50	2025.8	2529.3	503.71	2202.6	2706.3	1.5276	5.6020	7.1296	
125	0.23211	0.001065	0.7706	524.74	2009.9	2534.6	524.99	2188.5	2713.5	1.5813	5.4962	7.0775	
130	0.27010	0.001070	0.6685	546.02	1993.9	2539.9	546.31	2174.2	2720.5	1.6344	5.3925	7.0269	
135	0.31300	0.001075	0.5822	567.35	1977.7	2545.0	567.69	2159.6	2727.3	1.6870	5.2907	6.9777	
140	0.36133	0.001080	0.5089	588.74	1961.3	2550.0	589.13	2144.7	2733.9	1.7391	5.1908	6.9299	
145	0.41544	0.001085	0.4463	610.18	1944.7	2554.9	610.63	2129.6	2740.3	1.7907	5.0926	6.8833	
150	0.47588	0.001091	0.3928	631.68	1927.9	2559.5	632.20	2114.3	2746.5	1.8418	4.9960	6.8379	
155	0.54311	0.001096	0.3468	653.24	1910.8	2564.1	653.84	2098.6	2752.4	1.8925	4.9010	6.7935	
160	0.61788	0.001102	0.3071	674.87	1893.5	2568.4	675.55	2082.6	2758.1	1.9427	4.8075	6.7502	
165	0.70055	0.001108	0.2727	696.56	1876.0	2572.5	697.34	2066.2	2763.5	1.9925	4.7153	6.7078	
170	0.79177	0.001114	0.2428	718.33	1858.1	2576.5	719.21	2049.5	2768.7	2.0419	4.6244	6.6663	
175	0.89200	0.001121	0.2168	740.17	1840.0	2580.2	741.17	2032.4	2773.6	2.0909	4.5347	6.6256	
180	1.00211	0.001127	0.19405	762.09	1821.6	2583.7	763.22	2015.0	2778.2	2.1396	4.4461	6.5857	
185	1.12270	0.001134	0.17409	784.10	1802.9	2587.0	785.37	1997.1	2782.4	2.1879	4.3586	6.5465	
190	1.25444	0.001141	0.15654	806.19	1783.8	2590.0	807.62	1978.8	2786.4	2.2359	4.2720	6.5079	
195	1.39788	0.001149	0.14105	828.37	1764.4	2592.8	829.98	1960.0	2790.0	2.2835	4.1863	6.4698	
200	1.55388	0.001157	0.12736	850.65	1744.7	2595.3	852.45	1940.7	2793.2	2.3309	4.1014	6.4323	
205	1.72300	0.001164	0.11521	873.04	1724.5	2597.5	875.04	1921.0	2796.0	2.3780	4.0172	6.3952	
210	1.90622	0.001173	0.10441	895.53	1703.9	2599.5	897.76	1900.7	2798.5	2.4248	3.9337	6.3585	
215	2.10404	0.001181	0.09479	918.14	1682.9	2601.1	920.62	1879.9	2800.5	2.4714	3.8507	6.3221	
220	2.31800	0.001190	0.08619	940.87	1661.5	2602.4	943.62	1858.5	2802.1	2.5178	3.7683	6.2861	
225	2.54800	0.001199	0.07849	963.73	1639.6	2603.3	966.78	1836.5	2803.3	2.5639	3.6863	6.2503	
230	2.79500	0.001209	0.07158	986.74	1617.2	2603.9	990.12	1813.8	2804.0	2.6099	3.6047	6.2146	
235	3.06000	0.001219	0.06537	1009.89	1594.2	2604.1	1013.62	1790.5	2804.2	2.6558	3.5233	6.1791	
240	3.34400	0.001229	0.05976	1033.21	1570.8	2604.0	1037.32	1766.5	2803.8	2.7015	3.4422	6.1437	
245	3.64800	0.001240	0.05471	1056.71	1546.7	2603.4	1061.23	1741.7	2803.0	2.7472	3.3612	6.1083	

TABLE A.1 (SI) (cont'd.)

Temp. °C <i>T</i>	Press. MPa <i>P</i>	Specific Volume (m³/kg)						Internal Energy (kJ/kg)			Enthalpy (kJ/kg)			Entropy (kJ/kg · °K)		
		Sat. Liquid <i>v_f</i>	Sat. Vapor <i>v_g</i>	Sat. Liquid <i>u_f</i>	Sat. Vapor <i>u_g</i>	Sat. Liquid <i>h_f</i>	Sat. Vapor <i>h_g</i>	Sat. Liquid <i>s_f</i>	Sat. Vapor <i>s_g</i>	Sat. Liquid <i>h_g</i>	Sat. Vapor <i>h_f</i>	Sat. Liquid <i>s_f</i>	Sat. Vapor <i>s_g</i>			
25.0	3.973	0.001 25.1	0.050 13	1080.39	1522.0	2602.4	1085.36	1716.2	2801.5	2792.7	3.2802	3.2802	6.0730			
25.5	4.319	0.001 26.3	0.045 98	1104.28	1496.7	2600.9	1109.73	1689.8	2799.5	2.8383	3.1992	3.1992	6.0375			
26.0	4.688	0.001 27.6	0.042 21	1128.39	1470.6	2599.0	1134.37	1662.5	2796.9	2.8838	3.1181	3.1181	6.0019			
26.5	5.081	0.001 28.9	0.038 77	1152.74	1443.9	2596.6	1159.28	1634.4	2793.6	2.9294	3.0368	3.0368	5.9662			
27.0	5.499	0.001 30.2	0.035 64	1177.36	1416.3	2593.7	1184.51	1605.2	2789.7	2.9751	2.9551	2.9551	5.9301			
27.5	5.942	0.001 31.7	0.032 79	1202.25	1387.9	2590.2	1210.07	1574.9	2785.0	3.0208	2.8730	2.8730	5.8938			
28.0	6.412	0.001 33.2	0.030 17	1227.46	1358.7	2586.1	1235.99	1543.6	2779.6	3.0668	2.7903	2.7903	5.8571			
28.5	6.909	0.001 34.8	0.027 77	1253.00	1328.4	2581.4	1262.31	1511.0	2773.3	3.1130	2.7070	2.7070	5.8199			
29.0	7.436	0.001 36.6	0.025 57	1278.92	1297.1	2576.0	1289.07	1477.1	2766.2	3.1594	2.6227	2.6227	5.7821			
29.5	7.993	0.001 38.4	0.023 54	1305.2	1264.7	2569.9	1316.3	1441.8	2758.1	3.2062	2.5375	2.5375	5.7437			
30.0	8.581	0.001 40.4	0.021 67	1332.0	1231.0	2563.0	1344.0	1404.9	2749.0	3.2534	2.4511	2.4511	5.7045			
30.5	9.202	0.001 42.5	0.019 948	1359.3	1195.9	2555.2	1372.4	1366.4	2738.7	3.3010	2.3633	2.3633	5.6643			
31.0	9.856	0.001 44.7	0.018 350	1387.1	1159.4	2546.4	1401.3	1326.0	2727.3	3.3493	2.2737	2.2737	5.6230			
31.5	10.547	0.001 47.2	0.016 867	1415.5	1121.1	2536.6	1431.0	1283.5	2714.5	3.3982	2.1821	2.1821	5.5804			
32.0	11.274	0.001 49.9	0.015 488	1444.6	1080.9	2525.5	1461.5	1238.6	2700.1	3.4480	2.0882	2.0882	5.5362			
33.0	12.845	0.001 56.1	0.012 996	1505.3	993.7	2498.9	1525.3	1140.6	2665.9	3.5507	1.8909	1.8909	5.4417			
34.0	14.586	0.001 63.8	0.010 797	1570.3	894.3	2464.6	1594.2	1027.9	2622.0	3.6594	1.6763	1.6763	5.3357			
35.0	16.513	0.001 74.0	0.008 813	1641.9	776.6	2418.4	1670.6	893.4	2563.9	3.7777	1.4335	1.4335	5.2112			
36.0	18.651	0.001 893	0.006 945	1725.2	626.3	2351.5	1760.5	720.5	2481.0	3.9147	1.1379	1.1379	5.0526			
37.0	21.03	0.002 213	0.004 925	1844.0	384.5	2228.5	1890.5	441.6	2332.1	4.1106	.6865	.6865	4.7971			
374.14	22.09	0.003 155	0.003 155	2029.6	0	2029.6	2099.3	0	2099.3	4.4298	0	4.4298	0			

TABLE A.2 (SI)
Saturation Pressures (Steam)

Press. kPa <i>P</i>	Temp. °C <i>T</i>	Specific Volume (m ³ /kg)			Internal Energy (kJ/kg)			Enthalpy (kJ/kg)			Entropy (kJ/kg · °K)		
		Sat. Liquid <i>v_f</i>	Sat. Vapor <i>v_g</i>	Sat. Liquid <i>u_f</i>	Sat. Vapor <i>u_g</i>	Sat. Liquid <i>h_f</i>	Sat. Vapor <i>h_g</i>	Sat. Liquid <i>s_f</i>	Sat. Vapor <i>s_g</i>	Sat. Liquid <i>s_{f,g}</i>	Sat. Vapor <i>s_{f,g}</i>	Sat. Vapor <i>s_g</i>	
0.6113	0.01	0.001 000	206.14	.00	2375.3	2375.3	.01	2501.3	2501.4	.0000	9.1562	9.1562	
1.0	6.98	0.001 000	129.21	29.30	2355.7	2385.0	29.30	2484.9	2514.2	.1059	8.8697	8.9756	
1.5	13.03	0.001 001	87.98	54.71	2388.6	2393.3	54.71	2470.6	2525.3	.1957	8.6322	8.8279	
2.0	17.50	0.001 001	67.00	73.48	2326.0	2399.5	73.48	2460.0	2533.5	.2607	8.4629	8.7237	
2.5	21.08	0.001 002	54.25	88.48	2315.9	2404.4	88.49	2451.6	2540.0	.3120	8.3311	8.6432	
3.0	24.08	0.001 003	45.67	101.04	2307.5	2408.5	101.05	2444.5	2545.5	.3545	8.2231	8.5776	
4.0	28.96	0.001 004	34.80	121.45	2293.7	2415.2	121.46	2432.9	2554.4	.4226	8.0520	8.4746	
5.0	32.88	0.001 005	28.19	137.81	2282.7	2420.5	137.82	2423.7	2561.5	.4764	7.9187	8.3951	
7.5	40.29	0.001 008	19.24	168.78	2261.7	2430.5	168.79	2406.0	2574.8	.5764	7.6750	8.2515	
10	45.81	0.001 010	14.67	191.82	2246.1	2437.9	191.83	2392.8	2584.7	.6493	7.5009	8.1502	
15	53.97	0.001 014	10.02	225.92	2222.8	2448.7	*225.94	2373.1	2599.1	.7549	7.2536	8.0085	
20	60.06	0.001 017	7.649	251.38	2205.4	2456.7	251.40	2358.3	2609.7	.8320	7.0766	7.9085	
25	64.97	0.001 020	6.204	271.90	2191.2	2463.1	271.93	2346.3	2618.2	.8931	6.9383	7.8314	
30	69.10	0.001 022	5.229	289.20	2179.2	2468.4	289.23	2336.1	2625.3	.9439	6.8247	7.7686	
40	75.87	0.001 027	3.993	317.53	2159.5	2477.0	317.58	2319.2	2636.8	1.0259	6.6441	7.6700	
50	81.33	0.001 030	3.240	340.44	2143.4	2483.9	340.49	2305.4	2645.9	1.0910	6.5029	7.5939	
75	91.78	0.001 037	2.217	384.31	2112.4	2496.7	384.39	2278.6	2663.0	1.2130	6.2434	7.4564	
MPa													
0.100	99.63	0.001 043	1.6940	417.36	2088.7	2506.1	417.46	2258.0	2675.5	1.3026	6.0568	7.3594	
0.125	105.99	0.001 048	1.3749	444.19	2069.3	2513.5	444.32	2241.0	2685.4	1.3740	5.9104	7.2844	
0.150	111.37	0.001 053	1.1593	466.94	2052.7	2519.7	467.11	2226.5	2693.6	1.4336	5.7897	7.2233	
0.175	116.06	0.001 057	1.0036	486.80	2038.1	2524.9	486.99	2213.6	2700.6	1.4849	5.6868	7.1717	
0.200	120.23	0.001 061	0.8857	504.49	2025.0	2529.5	504.70	2201.9	2706.7	1.5301	5.5970	7.1271	
0.225	124.00	0.001 064	0.7933	520.47	2013.1	2533.6	520.72	2191.3	2712.1	1.5706	5.5173	7.0878	

TABLE A.2 (SI) (cont'd.)

Press. MPa <i>P</i>	Temp. °C <i>T</i>	Specific Volume			Internal Energy			Enthalpy			Entropy		
		Sat. Liquid <i>v_f</i>	Sat. Vapor <i>v_g</i>	Sat. Liquid <i>u_f</i>	Sat. Vapor <i>u_g</i>	Sat. Liquid <i>h_f</i>	Sat. Vapor <i>h_g</i>	Sat. Liquid <i>s_f</i>	Sat. Vapor <i>s_g</i>	Sat. Vapor <i>s_g</i>	Sat. Liquid <i>s_f</i>	Sat. Vapor <i>s_g</i>	
0.250	127.44	0.001 067	0.7187	535.10	2002.1	2537.2	535.37	2181.5	2716.9	1.6072	5.4455	7.0527	
0.275	130.60	0.001 070	0.6573	548.59	1991.9	2540.5	548.89	2172.4	2721.3	1.6408	5.3801	7.0209	
0.300	133.55	0.001 073	0.6058	561.15	1982.4	2543.6	561.47	2163.8	2725.3	1.6718	5.3201	6.9919	
0.325	136.30	0.001 076	0.5620	572.90	1973.5	2546.4	573.25	2155.8	2729.0	1.7006	5.2646	6.9652	
0.350	138.88	0.001 079	0.5243	583.95	1965.0	2548.9	584.33	2148.1	2732.4	1.7275	5.2130	6.9405	
0.375	141.32	0.001 081	0.4914	594.40	1956.9	2551.3	594.81	2140.8	2735.6	1.7528	5.1647	6.9175	
0.40	143.63	0.001 084	0.4625	604.31	1949.3	2553.6	604.74	2133.8	2738.6	1.7766	5.1193	6.8959	
0.45	147.93	0.001 088	0.4140	622.77	1934.9	2557.6	623.25	2120.7	2743.9	1.8207	5.0359	6.8565	
0.50	151.86	0.001 093	0.3749	639.68	1921.6	2561.2	640.23	2108.5	2748.7	1.8607	4.9606	6.8213	
0.55	155.48	0.001 097	0.3427	655.32	1909.2	2564.5	655.93	2097.0	2753.0	1.8973	4.8920	6.7893	
0.60	158.85	0.001 101	0.3157	669.90	1897.5	2567.4	670.56	2086.3	2756.8	1.9312	4.8288	6.7600	
0.65	162.01	0.001 104	0.2927	683.56	1886.5	2570.1	684.28	2076.0	2760.3	1.9627	4.7703	6.7331	
0.70	164.97	0.001 108	0.2729	696.44	1876.1	2572.5	697.22	2066.3	2763.5	1.9922	4.7158	6.7080	
0.75	167.78	0.001 112	0.2556	708.64	1866.1	2574.7	709.47	2057.0	2766.4	2.0200	4.6647	6.6847	
0.80	170.43	0.001 115	0.2404	720.22	1856.6	2576.8	721.11	2048.0	2769.1	2.0462	4.6166	6.6628	
0.85	172.96	0.001 118	0.2270	731.27	1847.4	2578.7	732.22	2039.4	2771.6	2.0710	4.5711	6.6421	
0.90	175.38	0.001 121	0.2150	741.83	1838.6	2580.5	742.83	2031.1	2773.9	2.0946	4.5280	6.6226	
0.95	177.69	0.001 124	0.2042	751.95	1830.2	2582.1	753.02	2023.1	2776.1	2.1172	4.4869	6.6041	
1.00	179.91	0.001 127	0.194 44	761.68	1822.0	2583.6	762.81	2015.3	2778.1	2.1387	4.4478	6.5865	
1.10	184.09	0.001 133	0.177 53	780.09	1806.3	2586.4	781.34	2000.4	2781.7	2.1792	4.3744	6.5536	
1.20	187.99	0.001 139	0.163 33	797.29	1791.5	2588.8	798.65	1986.2	2784.8	2.2166	4.3067	6.5233	
1.30	191.64	0.001 144	0.151 25	813.44	1777.5	2591.0	814.93	1972.7	2787.6	2.2515	4.2438	6.4953	
1.40	195.07	0.001 149	0.140 84	828.70	1764.1	2592.8	830.30	1959.7	2790.0	2.2842	4.1850	6.4693	

TABLE A.2 (SI) (cont'd.)

Press. MPa <i>P</i>	Temp. °C <i>T</i>	Specific Volume (m ³ /kg)			Internal Energy (kJ/kg)			Enthalpy (kJ/kg)			Entropy (kJ/kg · °K)		
		Sat. Liquid <i>v_f</i>	Sat. Vapor <i>v_g</i>	Sat. Liquid <i>u_f</i>	Sat. Vapor <i>u_g</i>	Sat. Evap. <i>u_{fg}</i>	Sat. Liquid <i>h_f</i>	Sat. Vapor <i>h_g</i>	Sat. Evap. <i>h_{fg}</i>	Sat. Liquid <i>s_f</i>	Sat. Vapor <i>s_g</i>	Sat. Evap. <i>s_{fg}</i>	
1.50	198.32	0.001 154	0.131 77	843.16	1751.3	2594.5	844.89	1947.3	2792.2	2.3150	4.1298	6.4448	
1.75	205.76	0.001 166	0.113 49	876.46	1721.4	2597.8	878.50	1917.9	2796.4	2.3851	4.0044	6.3896	
2.00	212.42	0.001 177	0.099 63	906.44	1693.8	2600.3	908.79	1890.7	2799.5	2.4474	3.8935	6.3409	
2.25	218.45	0.001 187	0.088 75	933.83	1668.2	2602.0	936.49	1865.2	2801.7	2.5035	3.7937	6.2972	
2.5	223.99	0.001 197	0.079 98	959.11	1644.0	2603.1	962.11	1841.0	2803.1	2.5547	3.7028	6.2575	
3.0	233.90	0.001 217	0.066 68	1004.78	1599.3	2604.1	1008.42	1795.7	2804.2	2.6457	3.5412	6.1869	
3.5	242.60	0.001 235	0.057 07	1045.43	1558.3	2603.7	1049.75	1753.7	2803.4	2.7253	3.4000	6.1253	
4	250.40	0.001 252	0.049 78	1082.31	1520.0	2602.3	1087.31	1714.1	2801.4	2.7964	3.2737	6.0701	
5	263.99	0.001 286	0.039 44	1147.81	1449.3	2597.1	1154.23	1640.1	2794.3	2.9202	3.0532	5.9734	
6	275.64	0.001 319	0.032 44	1205.44	1384.3	2589.7	1213.35	1571.0	2784.3	3.0267	2.8625	5.8892	
7	285.88	0.001 351	0.027 37	1257.55	1323.0	2580.5	1267.00	1505.1	2772.1	3.1211	2.6922	5.8133	
8	295.06	0.001 384	0.023 52	1305.57	1264.2	2569.8	1316.64	1441.3	2758.0	3.2068	2.5364	5.7432	
9	303.40	0.001 418	0.020 48	1350.51	1207.3	2557.8	1363.26	1378.9	2742.1	3.2858	2.3915	5.6772	
10	311.06	0.001 452	0.018 026	1393.04	1151.4	2544.4	1407.56	1317.1	2724.7	3.3596	2.2544	5.6141	
11	318.15	0.001 489	0.015 987	1433.7	1096.0	2529.8	1450.1	1255.5	2705.6	3.4295	2.1233	5.5527	
12	324.75	0.001 527	0.014 263	1473.0	1040.7	2513.7	1491.3	1193.6	2684.9	3.4962	1.9962	5.4924	
13	330.93	0.001 567	0.012 780	1511.1	985.0	2496.1	1531.5	1130.7	2662.2	3.5606	1.8718	5.4323	
14	336.75	0.001 611	0.011 485	1548.6	928.2	2476.8	1571.1	1066.5	2637.6	3.6232	1.7485	5.3717	
15	342.24	0.001 658	0.010 337	1585.6	869.8	2455.5	1610.5	1000.0	2610.5	3.6848	1.6249	5.3098	
16	347.44	0.001 711	0.009 306	1622.7	809.0	2431.7	1650.1	930.6	2580.6	3.7461	1.4994	5.2455	
17	352.37	0.001 770	0.008 364	1660.2	744.8	2405.0	1690.3	856.9	2547.2	3.8079	1.3698	5.1777	
18	357.06	0.001 840	0.007 489	1698.9	675.4	2374.3	1732.0	777.1	2509.1	3.8715	1.2329	5.1044	
19	361.54	0.001 924	0.006 657	1739.9	598.1	2338.1	1776.5	688.0	2464.5	3.9388	1.0839	5.0228	
20	365.81	0.002 036	0.005 834	1785.6	507.5	2293.0	1826.3	583.4	2409.7	4.0139	.9130	4.9269	
21	369.89	0.002 207	0.004 952	1842.1	388.5	2230.6	1888.4	446.2	2334.6	4.1075	.6938	4.8013	
22	373.80	0.002 742	0.003 568	1961.9	125.2	2087.1	2022.2	143.4	2165.6	4.3110	.2216	4.5327	
22.09	374.14	0.003 155	0.003 155	2029.6	0	2029.6	2099.3	0	2099.3	4.4298	0	4.4298	

TABLE A.3 (SI)
Properties of Superheated Steam

<i>P</i> = .010 MPa (45.81)						<i>P</i> = .050 MPa (81.33)						<i>P</i> = .10 MPa (99.63)							
<i>T</i>	<i>v</i>	<i>u</i>	<i>h</i>	<i>s</i>	<i>v</i>	<i>u</i>	<i>h</i>	<i>s</i>	<i>v</i>	<i>u</i>	<i>h</i>	<i>s</i>	<i>v</i>	<i>u</i>	<i>h</i>	<i>s</i>			
Sat.	14.674	2437.9	2584.7	8.1502	3.240	2483.9	2645.9	7.5939	1.6940	2506.1	2675.5	7.3594							
50	14.869	2443.9	2592.6	8.1749															
100	17.196	2515.5	2687.5	8.4479	3.418	2511.6	2682.5	7.6947	1.6958	2506.7	2676.2	7.3614							
150	19.512	2587.9	2783.0	8.6882	3.889	2585.6	2780.1	7.9401	1.9364	2582.8	2776.4	7.6134							
200	21.825	2661.3	2879.5	8.9038	4.356	2659.9	2877.7	8.1580	2.172	2658.1	2875.3	7.8343							
250	24.136	2736.0	2977.3	9.1002	4.820	2735.0	2976.0	8.3556	2.406	2733.7	2974.3	8.0333							
300	26.445	2812.1	3076.5	9.2813	5.284	2811.3	3075.5	8.5373	2.639	2810.4	3074.3	8.2158							
400	31.063	2968.9	3279.6	9.6077	6.209	2968.5	3278.9	8.8642	3.103	2967.9	3278.2	8.5435							
500	35.679	3132.3	3489.1	9.8978	7.134	3132.0	3488.7	9.1546	3.565	3131.6	3488.1	8.8342							
600	40.295	3302.5	3705.4	10.1608	8.057	3302.2	3705.1	9.4178	4.028	3301.9	3704.7	9.0976							
700	44.911	3479.6	3928.7	10.4028	8.981	3479.4	3928.5	9.6599	4.490	3479.2	3928.2	9.3398							
800	49.526	3663.8	4159.0	10.6281	9.904	3663.6	4158.9	9.8852	4.952	3663.5	4158.6	9.5652							
900	54.141	3855.0	4396.4	10.8396	10.828	3854.9	4396.3	10.0967	5.414	3854.8	4396.1	9.7767							
1000	58.757	4053.0	4640.6	11.0393	11.751	4052.9	4640.5	10.2964	5.875	4052.8	4640.3	9.9764							
1100	63.372	4257.5	4891.2	11.2287	12.674	4257.4	4891.1	10.4859	6.337	4257.3	4891.0	10.1659							
1200	67.987	4467.9	5147.8	11.4091	13.597	4467.8	5147.7	10.6662	6.799	4467.7	5147.6	10.3463							
1300	72.602	4683.7	5409.7	11.5811	14.521	4683.6	5409.6	10.8382	7.260	4683.5	5409.5	10.5183							
		<i>P</i> = .20 MPa (120.23)						<i>P</i> = .30 MPa (133.55)						<i>P</i> = .40 MPa (143.63)					
Sat.	.8857	2529.5	2706.7	7.1272	.6058	2543.6	2725.3	6.9919	.4625	2553.6	2738.6	6.8959							
150	.9596	2576.9	2768.8	7.2795	.6339	2570.8	2761.0	7.0778	.4708	2564.5	2752.8	6.9299							
200	1.0803	2654.4	2870.5	7.5066	.7163	2650.7	2865.6	7.3115	.5342	2646.8	2860.5	7.1706							
250	1.1988	2731.2	2971.0	7.7086	.7964	2728.7	2967.6	7.5166	.5951	2726.1	2964.2	7.3789							
300	1.3162	2808.6	3071.8	7.8926	.8753	2806.7	3069.3	7.7022	.6548	2804.8	3066.8	7.5662							
400	1.5493	2966.7	3276.6	8.2218	1.0315	2965.6	3275.0	8.0330	.7726	2964.4	3273.4	7.8985							

TABLE A.3 (SI) (cont'd.)

<i>T</i>	<i>v</i>	<i>u</i>	<i>h</i>	<i>s</i>	<i>v</i>	<i>u</i>	<i>h</i>	<i>s</i>	<i>P</i> = .30 MPa (133.55)			<i>P</i> = .40 MPa (143.63)		
									<i>v</i>	<i>u</i>	<i>h</i>	<i>s</i>	<i>v</i>	<i>u</i>
<i>P</i> = .20 MPa (120.23)														
500	1.7814	3130.8	3487.1	8.5133	1.1867	3130.0	3486.0	8.3251	.8893	3129.2	3484.9	8.1913		
600	2.013	3301.4	3704.0	8.7770	1.3414	3300.8	3703.2	8.5892	1.0055	3300.2	3702.4	8.4558		
700	2.244	3478.8	3927.6	9.0194	1.4957	3478.4	3927.1	8.8319	1.1215	3477.9	3926.5	8.6987		
800	2.475	3663.1	4158.2	9.2449	1.6499	3662.9	4157.8	9.0576	1.2372	3662.4	4157.3	8.9244		
900	2.706	3854.5	4395.8	9.4566	1.8041	3854.2	4395.4	9.2692	1.3529	3853.9	4395.1	9.1362		
1000	2.937	4052.5	4640.0	9.6563	1.9581	4052.3	4639.7	9.4690	1.4685	4052.0	4639.4	9.3360		
1100	3.168	4257.0	4890.7	9.8458	2.1121	4256.8	4890.4	9.6585	1.5840	4256.5	4890.2	9.5256		
1200	3.399	4467.5	5147.3	10.0262	2.2661	4467.2	5147.1	9.8389	1.6996	4467.0	5146.8	9.7060		
1300	3.630	4683.2	5409.3	10.1982	2.4201	4683.0	5409.0	10.0110	1.8151	4682.8	5408.8	9.8780		
<i>P</i> = .50 MPa (151.86)														
Sat.	.3749	2561.2	2748.7	6.8213	.3157	2567.4	2756.8	6.7600	.2404	2576.8	2769.1	6.6628		
200	.4249	2642.9	2855.4	7.0592	.3520	2638.9	2850.1	6.9665	.2608	2630.6	2839.3	6.8158		
250	.4744	2723.5	2960.7	7.2709	.3938	2720.9	2957.2	7.1816	.2931	2715.5	2950.0	7.0384		
300	.5226	2802.9	3064.2	7.4599	.4344	2801.0	3061.6	7.3724	.3241	2797.2	3056.5	7.2328		
350	.5701	2882.6	3167.7	7.6329	.4742	2881.2	3165.7	7.5464	.3544	2878.2	3161.7	7.4089		
400	.6173	2963.2	3271.9	7.7938	.5137	2962.1	3270.3	7.7079	.3843	2959.7	3267.1	7.5716		
500	.7109	3128.4	3483.9	8.0873	.5920	3127.6	3482.8	8.0021	.4433	3126.0	3480.6	7.8673		
600	.8041	3299.6	3701.7	7.3522	.6697	3299.1	3700.9	8.2674	.5018	3297.9	3699.4	8.1333		
700	.8969	3477.5	3925.9	8.5952	.7472	3477.0	3925.3	8.5107	.5601	3476.2	3924.2	8.3770		
800	.9896	3662.1	4156.9	8.8211	.8245	3661.8	4156.5	8.7367	.6181	3661.1	4155.6	8.6033		
900	1.0822	3853.6	4394.7	9.0329	.9017	3853.4	4394.4	8.9486	.6761	3852.8	4393.7	8.8153		
1000	1.1747	4051.8	4639.1	9.2328	.9788	4051.5	4638.8	9.1485	.7340	4051.0	4638.2	9.0153		
1100	1.2672	4256.3	4889.9	9.4224	1.0559	4256.1	4889.6	9.3381	.7919	4255.6	4889.1	9.2050		
1200	1.3596	4466.8	5146.6	9.6029	1.1330	4466.5	5146.3	9.5185	.8497	4466.1	5145.9	9.3855		
1300	1.4521	4682.5	5408.6	9.7749	1.2101	4682.3	5408.3	9.6906	.9076	4681.8	5407.9	9.5575		

TABLE A.3 (SI) (cont'd.)

<i>T</i>	<i>v</i>	<i>u</i>	<i>h</i>	<i>s</i>	<i>v</i>	<i>u</i>	<i>h</i>	<i>s</i>	<i>v</i>	<i>u</i>	<i>h</i>	<i>s</i>
<i>P</i> = 1.00 MPa (179.91)												
Sat.	.194 44	2583.6	2778.1	6.5865	.163 33	2583.8	2784.8	6.5233	.140 84	2592.8	2790.0	6.4693
200	.2060	2621.9	2827.9	6.6940	.169 30	2612.8	2815.9	6.5898	.143 02	2603.1	2803.3	6.4975
250	.2327	2709.9	2942.6	6.9247	.192 34	2704.2	2935.0	6.8294	.163 50	2698.3	2927.2	6.7467
300	.2579	2793.2	3051.2	7.1229	.2138	2789.2	3045.8	7.0317	.182 28	2785.2	3040.4	6.9534
350	.2825	2875.2	3157.7	7.3011	.2345	2872.2	3153.6	7.2121	.2003	2869.2	3149.5	7.1360
400	.3066	2957.3	3263.9	7.4651	.2548	2954.9	3260.7	7.3774	.2178	2952.5	3257.5	7.3026
500	.3541	3124.4	3478.5	7.7622	.2946	3122.8	3476.3	7.6759	.2521	3121.1	3474.1	7.6027
600	.4011	3296.8	3697.9	8.0290	.3339	3295.6	3696.3	7.9435	.2860	3294.4	3694.8	7.8710
700	.4478	3475.3	3923.1	8.2731	.3729	3474.4	3922.0	8.1881	.3195	3473.6	3920.8	8.1160
800	.4943	3660.4	4154.7	8.4996	.4118	3659.7	4153.8	8.4148	.3528	3659.0	4153.0	8.3431
900	.5407	3852.2	4392.9	8.7118	.4505	3851.6	4392.2	8.6272	.3861	3851.1	4391.5	8.5556
1000	.5871	4050.5	4637.6	8.9119	.4892	4050.0	4637.0	8.8274	.4192	4049.5	4636.4	8.7559
1100	.6335	4255.1	4888.6	9.1017	.5278	4254.6	4888.0	9.0172	.4524	4254.1	4887.5	8.9457
1200	.6798	4465.6	5145.4	9.2822	.5665	4465.1	5144.9	9.1977	.4855	4464.7	5144.4	9.1262
1300	.7261	4681.3	5407.4	9.4543	.6051	4680.9	5407.0	9.3698	.5186	4680.4	5406.5	9.2984
<i>P</i> = 1.60 MPa (201.41)												
Sat.	.123 80	2596.0	2794.0	6.4218	.110 42	2598.4	2797.1	6.3794	.099 63	2600.3	2799.5	6.3409
225	.132 87	2644.7	2857.3	6.5518	.116 73	2636.6	2846.7	6.4808	.103 77	2628.3	2835.8	6.4147
250	.141 84	2692.3	2919.2	6.6732	.124 97	2686.0	2911.0	6.6066	.111 44	2679.6	2902.5	6.5453
300	.158 62	2781.1	3034.8	6.8844	.140 21	2776.9	3029.2	6.8226	.125 47	2772.6	3023.5	6.7664
350	.174 56	2866.1	3145.4	7.0694	.154 57	2863.0	3141.2	7.0100	.138 57	2859.8	3137.0	6.9563
400	.190 05	2950.1	3254.2	7.2374	.168 47	2947.7	3250.9	7.1794	.151 20	2945.2	3247.6	7.1271
500	.2203	3119.5	3472.0	7.5390	.195 50	3117.9	3469.8	7.4825	.175 68	3116.2	3467.6	7.4317
600	.2500	3293.3	3693.2	7.8080	.2220	3292.1	3691.7	7.7523	.199 60	3290.9	3690.1	7.7024
700	.2794	3472.7	3919.7	8.0535	.2482	3471.8	3918.5	7.9983	.2332	3470.9	3917.4	7.9487
<i>P</i> = 1.80 MPa (207.15)												
Sat.	.123 80	2596.0	2794.0	6.4218	.110 42	2598.4	2797.1	6.3794	.099 63	2600.3	2799.5	6.3409
<i>P</i> = 2.00 MPa (212.42)												

TABLE A.3 (SI) (cont'd.)

<i>T</i>	<i>v</i>	<i>u</i>	<i>h</i>	<i>s</i>	<i>v</i>	<i>u</i>	<i>h</i>	<i>s</i>	<i>v</i>	<i>u</i>	<i>h</i>	<i>s</i>
<i>P</i> = 1.60 MPa (201.41)												
800	.3086	3658.3	4152.1	8.2808	.2742	3657.6	4151.2	8.2258	.2467	3657.0	4150.3	8.1765
900	.3377	3850.5	4390.8	8.4935	.3001	3849.9	4390.1	8.4386	.2700	3849.3	4389.4	8.3895
1000	.3668	4049.0	4635.8	8.6938	.3260	4048.5	4635.2	8.6391	.2933	4048.0	4634.6	8.5901
1100	.3958	4253.7	4887.0	8.8837	.3518	4253.2	4886.4	8.8290	.3166	4252.7	4885.9	8.7800
1200	.4248	4464.2	5143.9	9.0643	.3776	4463.7	5143.4	9.0096	.3398	4463.3	5142.9	8.9607
1300	.4538	4679.9	5406.0	9.2364	.4034	4679.5	5405.6	9.1818	.3631	4679.0	5405.1	9.1329
<i>P</i> = 1.80 MPa (207.15)												
Sat.	.079 98	2603.1	2803.1	6.2575	.066 68	2604.1	2804.2	6.1869	.057 07	2603.7	2803.4	6.1253
225	.080 27	2605.6	2806.3	6.2639	.070 58	2644.0	2855.8	6.2872	.058 72	2623.7	2829.2	6.1749
250	.087 00	2662.6	2880.1	6.4085	.081 14	2750.1	2993.5	6.5390	.068 42	2738.0	2977.5	6.4461
300	.098 90	2761.6	3008.8	6.6438	.090 53	2843.7	3115.3	6.7428	.076 78	2835.3	3104.0	6.6579
350	.109 76	2851.9	3126.3	6.8403	.099 36	2932.8	3230.9	6.9212	.084 53	2926.4	3222.3	6.8405
400	.120 10	2939.1	3239.3	7.0148	.107 87	3020.4	3344.0	7.0834	.091 96	3015.3	3337.2	7.0052
450	.130 14	3025.5	3350.8	7.1746	.116 19	3108.0	3456.5	7.2338	.099 18	3103.0	3450.9	7.1572
500	.139 98	3112.1	3462.1	7.3234	.132 43	3285.0	3682.3	7.5085	.113 24	3282.1	3678.4	7.4339
600	.159 30	3288.0	3686.3	7.5960	.148 38	3466.5	3911.7	7.7571	.126 99	3464.3	3908.8	7.6837
700	.178 32	3468.7	3914.5	7.8435	.164 14	3653.5	4145.9	7.9862	.140 56	3651.8	4143.7	7.9134
800	.197 16	3655.3	4148.2	8.0720	.179 80	3846.5	4385.9	8.1999	.154 02	3845.0	4384.1	8.1276
900	.215 90	3847.9	4387.6	8.2853	.195 41	4045.4	4631.6	8.4009	.167 43	4044.1	4630.1	8.3288
1000	.2346	4046.7	4633.1	8.4861	.210 98	4250.3	4883.3	8.5912	.180 80	4249.2	4881.9	8.5192
1100	.2532	4251.5	4884.6	8.6762	.226 52	4460.9	5140.5	8.7720	.194 15	4459.8	5139.3	8.7000
1200	.2718	4462.1	5141.7	8.8569	.242 06	4676.6	5402.8	8.9442	.207 49	4675.5	5401.7	8.8723
1300	.2905	4677.8	5404.0	9.0291								
<i>P</i> = 2.00 MPa (212.42)												
<i>P</i> = 2.50 MPa (223.99)												
<i>P</i> = 3.00 MPa (233.90)												
<i>P</i> = 3.50 MPa (242.60)												

TABLE A.3 (SI) (cont'd.)

<i>T</i>	<i>v</i>	<i>u</i>	<i>h</i>	<i>s</i>	<i>v</i>	<i>u</i>	<i>h</i>	<i>s</i>	<i>P</i> = 4.5 MPa (257.49)			<i>P</i> = 5.0 MPa (263.99)		
									<i>P</i> = 4.0 MPa (250.40)			<i>P</i> = 6.0 MPa (275.64)		
Sat.	.049 78	2602.3	2801.4	6.0701	.044 06	2600.1	2798.3	6.0198	.039 44	2597.1	2794.3	.039 44	2597.1	2794.3
275	.054 57	26667.9	2886.2	6.2285	.047 30	2650.3	2863.2	6.1401	.041 41	2631.3	2838.3	.041 41	2631.3	2838.3
300	.058 84	2725.3	2960.7	6.3615	.051 35	2712.0	2943.1	6.2828	.045 32	2698.0	2924.5	.045 32	2698.0	2924.5
350	.066 45	2826.7	3092.5	6.5821	.058 40	2817.8	3080.6	6.5131	.051 94	2808.7	3068.4	.051 94	2808.7	3068.4
400	.073 41	2919.9	3213.6	6.7690	.064 75	2913.3	3204.7	6.7047	.057 81	2906.6	3195.7	.057 81	2906.6	3195.7
450	.080 02	3010.2	3330.3	6.9363	.070 74	3005.0	3323.3	6.8746	.063 30	2999.7	3316.2	.063 30	2999.7	3316.2
500	.086 43	3099.5	3445.3	7.0901	.076 51	3095.3	3439.6	7.0301	.068 57	3091.0	3433.8	.068 57	3091.0	3433.8
600	.098 85	3279.1	3674.4	7.3688	.087 65	3276.0	3670.5	7.3110	.078 69	3273.0	3666.5	.078 69	3273.0	3666.5
700	.110 95	3462.1	3905.9	7.6198	.098 47	3459.9	3903.0	7.5631	.088 49	3457.6	3900.1	.088 49	3457.6	3900.1
800	.122 87	3650.0	4141.5	7.8502	.109 11	3648.3	4139.3	7.7942	.098 11	3646.6	4137.1	.098 11	3646.6	4137.1
900	.134 69	3843.6	4382.3	8.0647	.119 65	3842.2	4380.6	8.0091	.107 62	3840.7	4378.8	.107 62	3840.7	4378.8
1000	.146 45	4042.9	4628.7	8.2662	.130 13	4041.6	4627.2	8.2108	.117 07	4040.4	4625.7	.117 07	4040.4	4625.7
1100	.158 17	4248.0	4880.6	8.4567	.140 56	4246.8	4879.3	8.4015	.126 48	4245.6	4878.0	.126 48	4245.6	4878.0
1200	.169 87	4458.6	5138.1	8.6376	.150 98	4457.5	5136.9	8.5825	.135 87	4456.3	5135.7	.135 87	4456.3	5135.7
1300	.181 56	4674.3	5400.5	8.8100	.161 39	4673.1	5399.4	8.7549	.145 26	4672.0	5398.2	.145 26	4672.0	5398.2

TABLE A.3 (SI) (cont'd.)

<i>T</i>	<i>v</i>	<i>u</i>	<i>h</i>	<i>s</i>	<i>v</i>	<i>u</i>	<i>h</i>	<i>s</i>	<i>P</i> = 7.0 MPa (285.88)			<i>P</i> = 8.0 MPa (295.06)		
									<i>P</i> = 6.0 MPa (275.64)			<i>P</i> = 10.0 MPa (311.06)		
700	.073 52	3453.1	3894.2	7.4234	.062 83	3448.5	3888.3	7.3476	.054 81	3443.9	3882.4	7.2812		
800	.081 60	3643.1	4132.7	7.6566	.069 81	3639.5	4128.2	7.5822	.060 97	3636.0	4123.8	7.5173		
900	.089 58	3837.8	4375.3	7.8727	.076 69	3835.0	4371.8	7.7991	.067 02	3832.1	4368.3	7.7351		
1000	.097 49	4037.8	4622.7	8.0751	.083 50	4035.3	4619.8	8.0020	.073 01	4032.8	4616.9	7.9384		
1100	.105 36	4243.3	4875.4	8.2661	.090 27	4240.9	4872.8	8.1933	.078 96	4238.6	4870.3	8.1300		
1200	.113 21	4454.0	5133.3	8.4474	.097 03	4451.7	5130.9	8.3747	.084 89	4449.5	5128.5	8.3115		
1300	.121 06	4669.6	5396.0	8.6199	.103 77	4667.3	5393.7	8.5473	.090 80	4665.0	5391.5	8.4842		
Sat.														
325	.020 48	2557.8	2742.1	5.6772	.018 026	2544.4	2724.7	5.6141	.013 495	2505.1	2673.8	5.4624		
350	.023 27	2646.6	2856.0	5.8712	.019 861	2610.4	2809.1	5.7568						
400	.029 93	2848.4	3117.8	6.2854	.022 42	2699.2	2923.4	5.9443	.016 126	2624.6	2826.2	5.7118		
450	.033 50	2955.2	3256.6	6.4844	.026 41	2832.4	3096.5	6.2120	.020 00	2789.3	3039.3	6.0417		
500	.036 77	3055.2	3386.1	6.6576	.032 79	3045.8	3373.7	6.5966	.025 60	3021.7	3341.8	6.4618		
550	.039 87	3152.2	3511.0	6.8142	.035 64	3144.6	3500.9	6.7561	.028 01	3125.0	3475.2	6.6290		
600	.042 85	3248.1	3633.7	6.9589	.038 37	3241.7	3625.3	6.9029	.030 29	3225.4	3604.0	6.7810		
650	.045 74	3343.6	3755.3	7.0943	.041 01	3338.2	3748.2	7.0398	.032 48	3224.4	3730.4	6.9218		
700	.048 57	3439.3	3876.5	7.2221	.043 58	3434.7	3870.5	7.1687	.034 60	3422.9	3855.3	7.0536		
800	.054 09	3632.5	4119.3	7.4596	.048 59	3628.9	4114.8	7.4077	.038 69	3620.0	4103.6	7.2965		
900	.059 50	3829.2	4364.8	7.6783	.053 49	3826.3	4361.2	7.6272	.042 67	3819.1	4352.5	7.5182		
1000	.064 85	4030.3	4614.0	7.8821	.058 32	4027.8	4611.0	7.8315	.046 58	4021.6	4603.8	7.7237		
1100	.070 16	4236.3	4867.7	8.0740	.063 12	4234.0	4865.1	8.0237	.050 45	4228.2	4858.8	7.9165		
1200	.075 44	4447.2	5126.2	8.2556	.067 89	4444.9	5123.8	8.2055	.054 30	4439.3	5118.0	8.0987		
1300	.080 72	4662.7	5389.2	8.4284	.072 65	4460.5	5387.0	8.3783	.058 13	4654.8	5381.4	8.2717		

TABLE A.3 (S1) (cont'd.)

<i>T</i>	<i>v</i>	<i>u</i>	<i>h</i>	<i>s</i>	<i>v</i>	<i>u</i>	<i>h</i>	<i>s</i>	<i>P</i> = 15.0 MPa (342.24)		<i>P</i> = 17.5 MPa (354.75)		<i>P</i> = 20.0 MPa (365.81)		
									<i>P</i> = 20.0 MPa (365.81)						
Sat.	.010 337	2455.5	2610.5	5.3098	.007 920	2390.2	2528.8	5.1419	.005 834	2293.0	2409.7	.005 834	2293.0	2409.7	4.9269
350	.011 470	2520.4	2692.4	5.4421	.012 447	2685.0	2902.9	5.7213	.009 942	2619.3	2818.1	.012 695	2806.2	3060.1	5.5540
400	.015 649	2740.7	2975.5	5.8811	.015 174	2844.2	3109.7	6.0184	.012 695	2942.9	3238.2	.014 768	2942.9	3238.2	5.9017
450	.018 445	2879.5	3156.2	6.1404	.017 358	2970.3	3274.1	6.2383	.016 555	3062.4	3393.5	.018 178	3174.0	3537.6	6.1401
500	.020 80	2996.6	3308.6	6.3443	.019 288	3083.9	3421.4	6.4230	.016 555	3062.4	3393.5	.019 693	3281.4	3675.3	6.3348
550	.022 93	3104.7	3448.6	6.5199	.021 06	3191.5	3560.1	6.5866	.018 178	3174.0	3537.6	.021 13	3386.4	3809.0	6.5048
600	.024 91	3208.6	3582.3	6.6776	.022 74	3296.0	3693.9	6.7357	.019 693	3281.4	3675.3	.023 85	3592.7	4069.7	6.6582
650	.026 80	3310.3	3712.3	6.8224	.024 34	3398.7	3824.6	6.8736	.021 13	3386.4	3809.0	.024 45	3797.5	4326.4	7.0544
700	.028 61	3410.9	3840.1	6.9572	.027 38	3601.8	4081.1	7.1244	.023 85	3592.7	4069.7	.026 45	3797.5	4326.4	7.2830
800	.032 10	3610.9	4092.4	7.2040	.030 31	3804.7	4335.1	7.3507	.026 45	3797.5	4326.4	.028 97	4003.1	4582.5	7.4925
900	.035 46	3811.9	4343.8	7.4279	.033 16	4009.3	4589.5	7.5589	.028 97	4003.1	4582.5	.031 45	4211.3	4840.2	7.6874
1000	.038 75	4015.4	4596.6	7.6348	.035 97	4216.9	4846.4	7.7531	.033 91	4422.8	5101.0	.036 36	4638.0	5365.1	8.0442
1100	.042 00	4222.6	4852.6	7.8283	.038 76	4428.3	5106.6	7.9360	.038 91	4422.8	5101.0	.041 54	4643.5	5370.5	
1200	.045 23	4433.8	5112.3	8.0108	.041 54	4649.1	5376.0	8.1840	.041 54	4649.1	5376.0	.045 23	4852.6	5596.6	
1300	.048 45	4649.1	5376.0	8.3356	.045 23	4852.6	5596.6	8.5108	.045 23	4852.6	5596.6	.050 00	5112.3	5846.4	
<i>P</i> = 25.0 MPa														<i>P</i> = 30.0 MPa	<i>P</i> = 35.0 MPa
375	.001 973	1	1798.7	1848.0	4.0320	.001 789	2	1737.8	1791.5	3.9305	.001 700	3	1702.9	1762.4	3.8722
400	.006 004	2430.1	2580.2	5.1418	.002 790	2067.4	2151.1	4.4728	.002 100	1914.1	1987.6	.003 428	2253.4	2373.4	4.2126
425	.007 881	2609.2	2806.3	5.4723	.005 303	2455.1	2614.2	5.1504	.004 961	2498.7	2672.4	.006 927	2751.9	2994.4	4.7747
450	.009 162	2720.7	2949.7	5.6744	.006 735	2619.3	2821.4	5.4424	.004 961	2498.7	2672.4	.008 345	2921.0	3213.0	5.1962
500	.011 123	2884.3	3162.4	5.9592	.008 678	2820.7	3081.1	5.7905	.006 927	2751.9	2994.4	.010 575	3062.0	3395.5	5.6282
550	.012 724	3017.5	3335.6	6.1765	.010 168	2970.3	3275.4	6.0342	.008 345	2921.0	3213.0	.012 695	3395.5	3559.9	6.3010
600	.014 137	3137.9	3491.4	6.3602	.011 446	3100.5	3443.9	6.2331	.009 527	3062.0	3395.5	.014 768	3559.9	3809.0	
650	.015 433	3251.6	3637.4	6.5229	.012 596	3221.0	3598.9	6.4058	.010 575	3189.8	3559.9	.016 801	3809.0	4069.7	

TABLE A.3 (SI) (cont'd.)

<i>T</i>	<i>v</i>	<i>u</i>	<i>h</i>	<i>s</i>	<i>v</i>	<i>u</i>	<i>h</i>	<i>s</i>	<i>P</i> = 30.0 MPa			<i>P</i> = 35.0 MPa			
									<i>P</i> = 25.0 MPa			<i>P</i> = 30.0 MPa			
700	.016 646	3361.3	3777.5	6.6707	.013 661	3335.8	3745.6	6.5606	.011 533	3309.8	3713.5	6.4631			
800	.018 912	3574.3	4047.1	6.9345	.015 623	3555.5	4024.2	6.8332	.013 278	3536.7	4001.5	6.7450			
900	.021 045	3783.0	4309.1	7.1680	.017 448	3768.5	4291.9	7.0718	.014 883	3754.0	4274.9	6.9886			
1000	.023 10	3990.9	4568.5	7.3802	.019 196	3978.8	4554.7	7.2867	.016 410	3966.7	4541.1	7.2064			
1100	.025 12	4200.2	4828.2	7.5765	.020 903	4189.2	4816.3	7.4845	.017 895	4178.3	4804.6	7.4057			
1200	.027 11	4412.0	5089.9	7.7605	.022 589	4401.3	5079.0	7.6692	.019 360	4390.7	5068.3	7.5910			
1300	.029 10	4626.9	5354.4	7.9342	.024 266	4616.0	5344.0	7.8432	.020 815	4605.1	5333.6	7.7653			
P = 40.0 MPa														P = 60.0 MPa	
375	.001 640 7	1677.1	1742.8	3.8290	.001 559 4	1638.6	1716.6	3.7639	.001 502 8	1609.4	1699.5	3.7141			
400	.001 907 7	1854.6	1930.9	4.1135	.001 730 9	1788.1	1874.6	4.0031	.001 633 5	1745.4	1843.4	3.9318			
425	.002 532	2096.9	2198.1	4.5029	.002 007	1959.7	2060.0	4.2734	.001 816 5	1892.7	2001.7	4.1626			
450	.003 693	2365.1	2512.8	4.9459	.002 486	2159.6	2284.0	4.5884	.002 085	2053.9	2179.0	4.4121			
500	.005 622	2678.4	2903.3	5.4700	.003 892	2525.5	2720.1	5.1726	.002 956	2390.6	2567.9	4.9321			
550	.006 984	2869.7	3149.1	5.7785	.005 118	2763.6	3019.5	5.5485	.003 956	2658.8	2896.2	5.3441			
600	.008 094	3022.6	3346.4	6.0114	.006 112	2942.0	3247.6	5.8178	.004 834	2861.1	3151.2	5.6452			
650	.009 063	3158.0	3520.6	6.2054	.006 966	3093.5	3441.8	6.0342	.005 595	3028.8	3364.5	5.8829			
700	.009 941	3283.6	3681.2	6.3750	.007 727	3230.5	3616.8	6.2189	.006 272	3177.2	3553.5	6.0824			
800	.011 523	3517.8	3978.7	6.6662	.009 076	3479.8	3933.6	6.5290	.007 459	3441.5	3889.1	6.4109			
900	.012 962	3739.4	4257.9	6.9150	.010 283	3710.3	4224.4	6.7882	.008 508	3681.0	4191.5	6.6805			
1000	.014 324	3954.6	4527.6	7.1356	.011 411	3930.5	4501.1	7.0146	.009 480	3906.4	4475.2	6.9127			
1100	.015 642	4167.4	4793.1	7.3364	.012 496	4145.7	4770.5	7.2184	.010 409	4124.1	4748.6	7.1195			
1200	.016 940	4380.1	5057.7	7.5224	.013 561	4359.1	5037.2	7.4058	.011 317	4338.2	5017.2	7.3083			
1300	.018 229	4594.3	5323.5	7.6969	.014 616	4572.8	5303.6	7.5808	.012 215	4551.4	5284.3	7.4837			

TABLE 4

t	p (t Sat.) MPa	0						2.5 (2223.99)						5.0 (2633.99)					
		$10^3 v$	u	h	s	$10^3 v$	u	h	s	$10^3 v$	u	h	s	$10^3 v$	u	h	s		
Sat.																			
0	1.0002	-0.03	-0.03	-0.0001	0.9990	-0.00	2.50	-0.0000	0.9977	0.04	5.04	0.0001							
20	1.0018	83.95	83.95	0.2966	1.0006	83.80	86.30	0.2961	0.9995	83.65	88.65	0.2956							
40	1.0078	167.56	167.56	0.5725	1.0067	167.25	169.77	0.5715	1.0056	166.95	171.97	0.5705							
60	1.0172	251.12	251.12	0.8312	1.0160	250.67	253.21	0.8298	1.0149	250.23	255.30	0.8285							
80	1.1291	334.87	334.87	1.0753	1.0280	334.29	336.86	1.0737	1.0268	333.72	338.85	1.0720							
100	1.0436	418.96	418.96	1.3069	1.0423	418.24	420.85	1.3050	1.0410	417.52	422.72	1.3030							
120	1.0604	503.57	503.57	1.5278	1.0590	502.68	505.33	1.5255	1.0576	501.80	507.09	1.5233							
140	1.0800	588.89	588.89	1.7395	1.0784	587.82	590.52	1.7369	1.0768	586.76	592.15	1.7343							
160	1.1024	675.19	675.19	1.9434	1.1006	673.90	676.65	1.9404	1.0988	672.62	678.12	1.9375							
180	1.1283	762.72	762.72	2.1410	1.1261	761.16	763.97	2.1375	1.1240	759.63	765.25	2.1341							
200	1.1581	851.8	851.8	2.3334	1.1555	849.9	852.8	2.3294	1.1530	848.1	853.9	2.3255							
210	1.1749	897.1	897.1	2.4281	1.1720	895.0	898.0	2.4238	1.1691	893.0	898.8	2.4195							
220	1.1930	943.0	943.0	2.5221	1.1898	940.7	943.7	2.5174	1.1866	938.4	944.4	2.5128							
230	1.2129	989.6	989.6	2.6157	1.2092	987.0	990.1	2.6105	1.2056	984.5	990.6	2.6055							
240	1.2347	1037.1	1037.1	2.7091	1.2305	1034.2	1037.2	2.7034	1.2264	1031.4	1037.5	2.6979							
250	1.2590	1085.6	1085.6	2.8027	1.2540	1082.3	1085.4	2.7964	1.2493	1079.1	1085.3	2.7902							
260	1.2862	1135.4	1135.4	2.8970	1.2804	1131.6	1134.8	2.8898	1.2749	1127.9	1134.3	2.8830							
270	1.3173	1186.8	1186.8	2.9926	1.3102	1182.4	1185.7	2.9844	1.3036	1178.2	1184.3	2.9766							
280	1.3535	1240.4	1240.4	3.0904	1.3447	1235.1	1238.5	3.0808	1.3365	1230.2	1236.8	3.0717							
290	1.3971	1297.0	1297.0	3.1918	1.3855	1290.5	1294.0	3.1801	1.3750	1284.4	1291.3	3.1693							
300	1.4520	1358.1	1358.1	3.2992	1.4357	1349.6	1353.2	3.2843	1.4214	1341.9	1349.0	3.2708							
310										1.4803	1404.1	1411.5	3.3789						

5.3 THERMODYNAMIC PROPERTIES OF STEAM 201

FIGURE 5.11a Extract from subcooled table (SI units).

TABLE A.4 (SI)
Properties of Compressed Liquid (Steam)

<i>T</i>	<i>P</i> = 5 MPa (263.99)				<i>P</i> = 10 MPa (311.06)				<i>P</i> = 15 MPa (342.24)			
	<i>v</i>	<i>u</i>	<i>h</i>	<i>s</i>	<i>v</i>	<i>u</i>	<i>h</i>	<i>s</i>	<i>v</i>	<i>u</i>	<i>h</i>	<i>s</i>
Sat.	.001 285.9	1147.8	1154.2	2.9202	.001 452.4	1393.0	1407.6	3.3596	.001 658.1	1585.6	1610.5	3.6848
0	.000 997.7	.04	5.04	.0001	.000 995.2	.09	10.04	.0002	.000 992.8	.15	15.05	.0004
20	.000 999.5	83.65	88.65	.2956	.000 997.2	83.36	93.33	.2945	.000 995.0	83.06	97.99	.2934
40	.001 005.6	166.95	171.97	.5705	.001 003.4	166.35	176.38	.5686	.001 001.3	165.76	180.78	.5666
60	.001 014.9	250.23	255.30	.8285	.001 012.7	249.36	259.49	.8258	.001 010.5	248.51	263.67	.8232
80	.001 026.8	333.72	338.85	1.0720	.001 024.5	332.59	342.83	1.0688	.001 022.2	331.48	346.81	1.0656
100	.001 041.0	417.52	422.72	1.3030	.001 038.5	416.12	426.50	1.2992	.001 036.1	414.74	430.28	1.2955
120	.001 057.6	501.80	507.09	1.5233	.001 054.9	500.08	510.64	1.5189	.001 052.2	498.40	514.19	1.5145
140	.001 076.8	586.76	592.15	1.7343	.001 073.7	584.68	595.42	1.7292	.001 070.7	582.66	598.72	1.7242
160	.001 098.8	672.62	678.12	1.9375	.001 095.3	670.13	681.08	1.9317	.001 091.8	667.71	684.09	1.9260
180	.001 124.0	759.63	765.25	2.1341	.001 119.9	756.65	767.84	2.1275	.001 115.9	753.76	770.50	2.1210
200	.001 153.0	848.1	853.9	2.3255	.001 148.0	844.5	856.0	2.3178	.001 143.3	841.0	858.2	2.3104
220	.001 186.6	938.4	944.4	2.5128	.001 180.5	934.1	945.9	2.5039	.001 174.8	929.9	947.5	2.4953
240	.001 226.4	1031.4	1037.5	2.6979	.001 218.7	1026.0	1038.1	2.6872	.001 211.4	1020.8	1039.0	2.6771
260	.001 274.9	1134.3	1134.3	2.8830	.001 264.5	1121.1	1133.7	2.8699	.001 255.0	1114.6	1133.4	2.8576
280					.001 321.6	1220.9	1234.1	3.0548	.001 308.4	1212.5	1232.1	3.0393
300					.001 397.2	1328.4	1342.3	3.2469	.001 377.0	1316.6	1337.3	3.2260
320									.001 472.4	1431.1	1453.2	3.4247
340									.001 631.1	1567.5	1591.9	3.6546

TABLE A.4 (S1) (cont'd.)

<i>T</i>	<i>P</i> = 20 MPa (365.81)			<i>P</i> = 30 MPa			<i>P</i> = 50 MPa					
	<i>v</i>	<i>u</i>	<i>h</i>	<i>s</i>	<i>v</i>	<i>u</i>	<i>h</i>	<i>s</i>	<i>v</i>	<i>u</i>	<i>h</i>	<i>s</i>
Sat.	.002 036	1785.6	1826.3	4.0139								
0	.000 990 4	.19	20.01	.0004	.000 985 6	.25	29.82	.0001	.000 976 6	.20	49.03	.0014
20	.000 992 8	82.77	102.62	.2923	.000 988 6	82.17	111.84	.2899	.000 980 4	81.00	130.02	.2848
40	.000 999 2	165.17	185.16	.5646	.000 995 1	164.04	193.89	.5607	.000 987 2	161.86	211.21	.5527
60	.001 008 4	247.68	267.85	.8206	.001 004 2	246.06	276.19	.8154	.000 996 2	242.98	292.79	.8052
80	.001 019 9	330.40	350.80	1.0624	.001 015 6	328.30	358.77	1.0561	.001 007 3	324.34	374.70	1.0440
100	.001 033 7	413.39	434.06	1.2917	.001 029 0	410.78	441.66	1.2844	.001 020 1	405.88	456.89	1.2703
120	.001 049 6	496.76	517.76	1.5102	.001 044 5	493.59	524.93	1.5018	.001 034 8	487.65	539.39	1.4857
140	.001 067 8	580.69	602.04	1.7193	.001 062 1	576.88	608.75	1.7098	.001 051 5	569.77	622.35	1.6915
160	.001 088 5	665.35	687.12	1.9204	.001 082 1	660.82	693.28	1.9096	.001 070 3	652.41	705.92	1.8891
180	.001 112 0	750.95	773.20	2.1147	.001 104 7	745.59	778.73	2.1024	.001 091 2	735.69	790.25	2.0794
200	.001 138 8	837.7	860.5	2.3031	.001 130 2	831.4	865.3	2.2893	.001 114 6	819.7	875.5	2.2634
220	.001 169 3	925.9	949.3	2.4870	.001 159 0	918.3	953.1	2.4711	.001 140 8	904.7	961.7	2.4419
240	.001 204 6	1016.0	1040.0	2.6674	.001 192 0	1006.9	1042.6	2.6490	.001 170 2	990.7	1049.2	2.6158
260	.001 246 2	1108.6	1133.5	2.8459	.001 230 3	1097.4	1134.3	2.8243	.001 203 4	1078.1	1138.2	2.7860
280	.001 296 5	1204.7	1230.6	3.0248	.001 275 5	1190.7	1229.0	2.9986	.001 241 5	1167.2	1229.3	2.9537
300	.001 359 6	1306.1	1333.3	3.2071	.001 330 4	1287.9	1327.8	3.1741	.001 286 0	1258.7	1323.0	3.1200
320	.001 443 7	1415.7	1444.6	3.3979	.001 399 7	1390.7	1432.7	3.3539	.001 338 8	1353.3	1420.2	3.2868
340	.001 568 4	1539.7	1571.0	3.6075	.001 492 0	1501.7	1546.5	3.5426	.001 403 2	1452.0	1522.1	3.4557
360	.001 822 6	1702.8	1739.3	3.8772	.001 626 5	1626.6	1675.4	3.7494	.001 483 3	1556.0	1630.2	3.6291
380					.001 869 1	1781.4	1837.5	4.0012	.001 588 4	1667.2	1746.6	3.8101